

Stochastic Immersed Boundary Methods

April 2021

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DOE ASCR CM4
DE-SC0009254



DOE ASCR PhilMS
DE-SC0019246



NSF Grant
DMS - 1616353

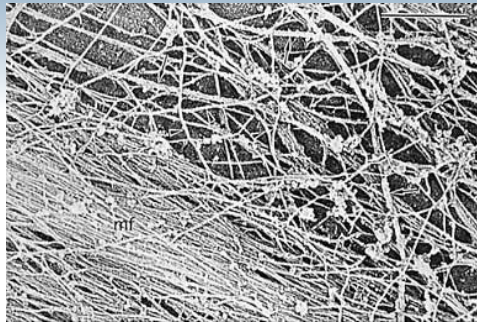


NSF CAREER Grant
DMS-0956210

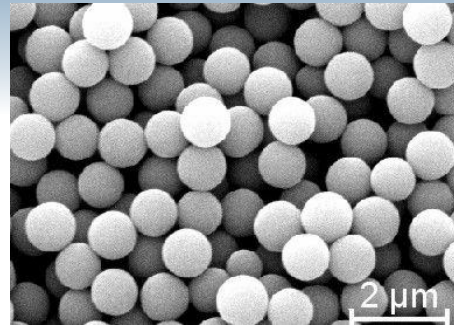
Stochastic Immersed Boundary Methods

Motivations

Motivations: Soft Materials, Complex Fluids, and Other Applications



Gels (Actin)



Colloids



Membranes (lipids)

Soft Materials / Complex Fluids

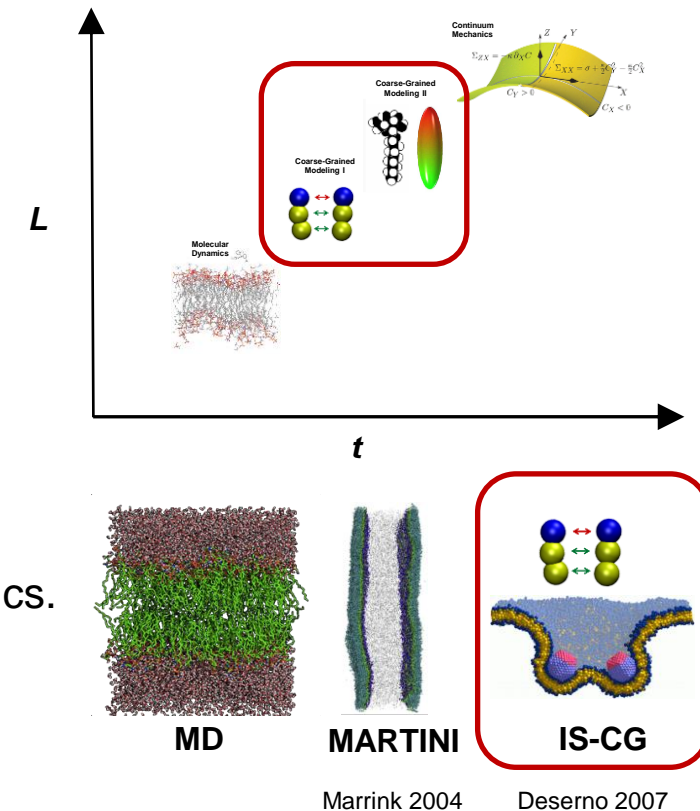
- Microstructure interactions on the order of $K_B T$.
- Properties arise from balance of entropy-enthalpy.
- Solvent plays important role (interactions / dynamic responses).

Approaches

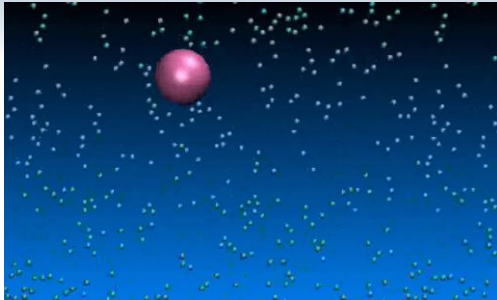
- Atomistic Molecular Dynamics.
- Continuum Mechanics.
- Coarse-Grained Particle Models (solvated or implicitly treated).
- Challenges from phenomena spanning wide temporal-spatial scales.

Simulation Aims

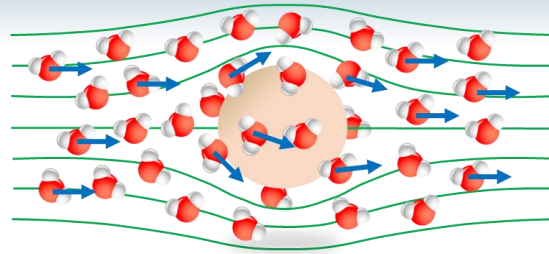
- Investigate how larger-scale mechanics arise from microstructure interactions / kinetics.
- Capture roles of solvent mediated interactions efficiently (i.e. continuum level).
- Resolve microstructure mechanics and dynamics.
- Computational efficiencies allow for accessing larger length and time-scales for investigating wider class of phenomena.



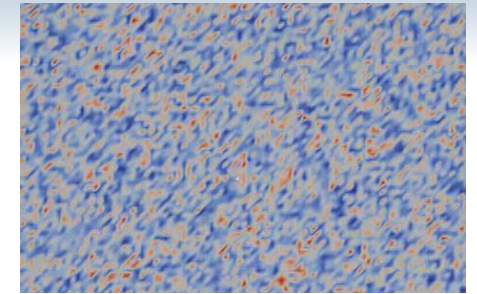
Fluctuating Hydrodynamics



Brownian Motion: Molecular Collisions



Hydrodynamics + Fluctuations



Continuum Gaussian Random Field

Landau-Lifschitz fluctuating hydrodynamics

$$\rho \left(\frac{\partial \mathbf{u}(\mathbf{x}, t)}{\partial t} + \mathbf{u}(\mathbf{x}, t) \cdot \nabla \mathbf{u}(\mathbf{x}, t) \right) = \mu \Delta \mathbf{u}(\mathbf{x}, t) - \nabla p(\mathbf{x}, t) + \nabla \cdot \Sigma(\mathbf{x}, t).$$

$$\nabla \cdot \mathbf{u}(\mathbf{x}, t) = 0.$$

$$\langle \Sigma_{ij}(\mathbf{x}, t) \Sigma_{kl}(\mathbf{y}, s) \rangle = 2\mu k_B T (\delta_{ik} \delta_{jl} + \delta_{il} \delta_{jk}) \delta(\mathbf{x} - \mathbf{y}) \delta(t - s).$$

Landau ~1959

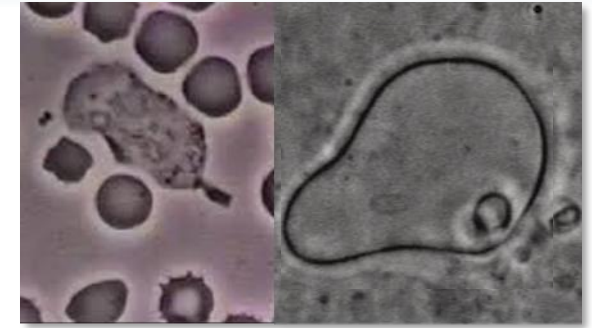
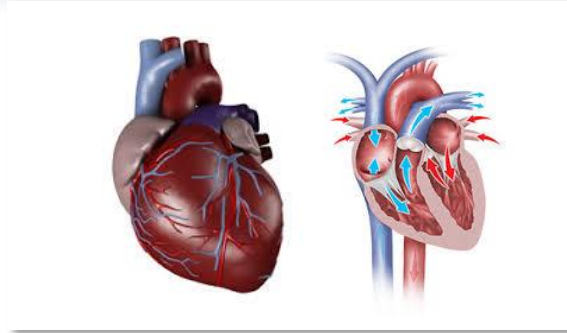
Fluctuations arise from spontaneous momentum transfer from molecular-level collisions.

Stochastic model of thermal fluctuations captured through random stress $\Sigma \sim$ Gaussian.

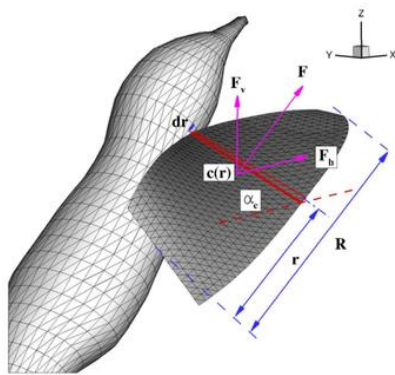
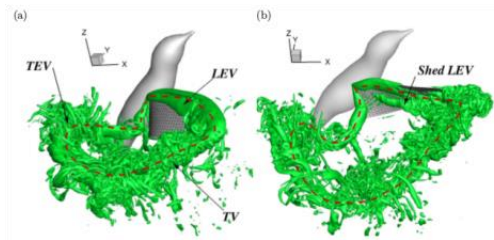
Challenges for analysis and numerical methods presented from the δ -correlation in space-time.

Fluid-structure interactions: How to incorporate tractably?

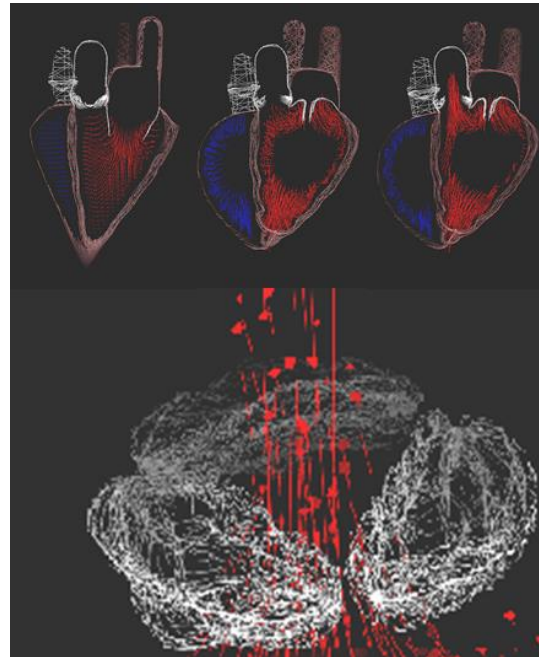
Fluid-Structure Interactions



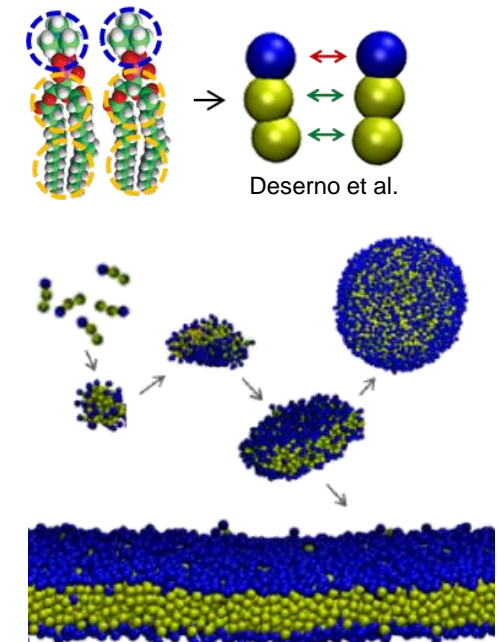
David Rogers



Song, J., Luo, H., Hedrick, T.L.



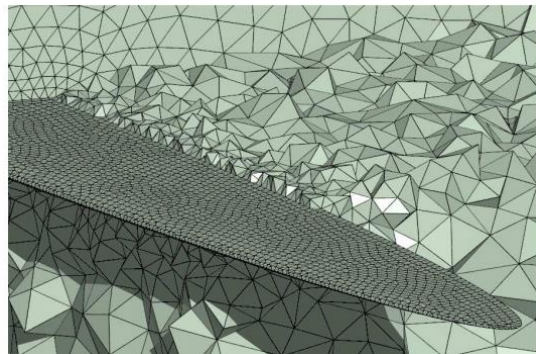
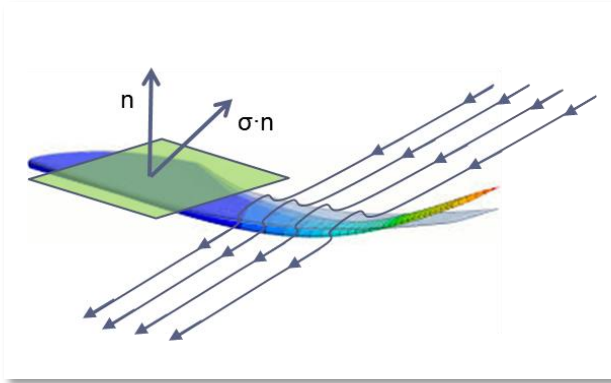
Peskin, C and McQueen, D. et al.
Griffith et al.



Atzberger, P., Sigurdsson, J. et al.

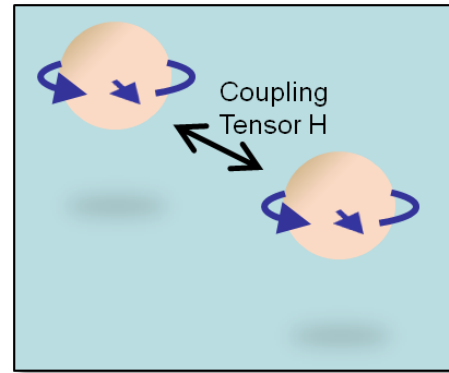
CFD : Approaches

Boundary Coupling



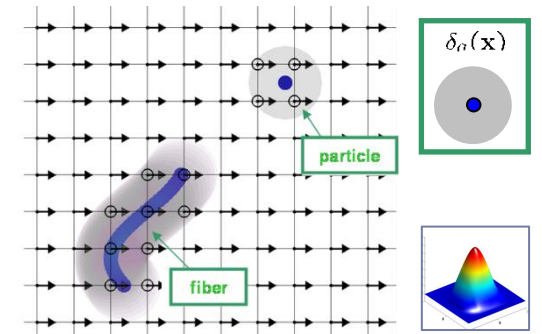
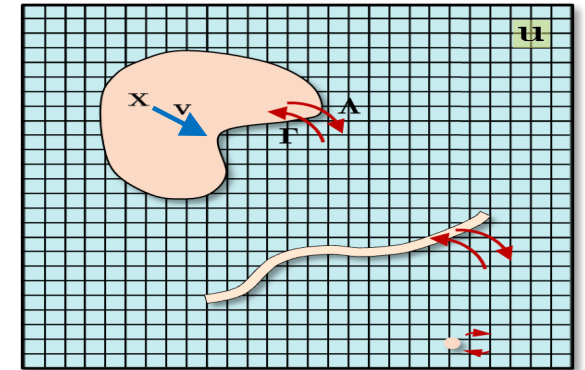
J. Peraire and P.-O. Persson

Coupling Tensor



Brady et al., G. Gompper et al.

IB Eulerian-Lagrangian



Atzberger, Peskin, Kramer 2007

Stochastic Immersed Boundary Methods

Background:
Statistical Mechanics
Stochastic Analysis

Background

Equilibrium Statistical Mechanics (Canonical Ensemble)

Consider a system with states X which have energy $E[X]$. At equilibrium in the NVT ensemble, the probability of observing state X is given by

$$\rho(X) = \frac{1}{Z} \exp \left[-\frac{E[X]}{k_B T} \right].$$

The Z is the *partition function* $Z = \int_{\Omega} \exp(-E/k_B T) dX$, k_B is Boltzmann's constant, T is temperature.

Fluctuation-Dissipation Principle

A spontaneous perturbation of the system due to fluctuations relaxes the same way as a small externally induced perturbation of the system.

Stochastic Differential Equations (SDEs) and Dynamics

The dynamics of many systems can be modeled using Stochastic Differential Equations (SDEs) of the general form

$$dX_t = a(X_t)dt + b(X_t)dW_t.$$

Here, we use Ito's interpretation with $a(x)$ giving the drift, b the covariance, and dW_t increments of the Weiner process.

Ito's Lemma

Consider the Stochastic Differential Equation (SDE)

$$dX_t = a(X_t)dt + b(X_t)dW_t$$

with the change of variable $Y_t = f(X_t)$ with $f \in C^2(\Omega)$. The process Y_t satisfies the SDE given by

$$dY_t = \nabla f(X_t)dX_t + \frac{1}{2}dX_t^T \nabla^2 f(X_t)dX_t,$$

with conventions $[dW_t]_i [dW_t]_j = \delta_{ij} dt$ and $dt dt = 0 = dt [dW_t]_i$. More explicitly, we can express this as

$$dY_t = \left(\nabla f(X_t)a(X_t) + \frac{1}{2} \text{Tr} \left[b(X_t)^T \nabla^2 f(X_t)b(X_t) \right] \right) dt + \nabla f(X_t)b(X_t)dW_t.$$

Fluctuation-Dissipation Principle and Ito's Lemma

Consider a system with energy $E[X] = \frac{1}{2}X^T C^{-1}X$ that has linear dynamics $dX_t = LX_t dt + QdW_t$. To obtain the equilibrium (steady-state) probability density $\rho(X) = (1/Z) \exp \left[-\frac{E[X]}{k_B T} \right]$ we must have that

$$QQ^T = -LC - C^T L^T.$$

Background

Fluctuation-Dissipation Principle and Ito's Lemma

Consider a system with energy $E[X] = \frac{1}{2}X^T C^{-1}X$ that has linear dynamics $dX_t = LX_t dt + QdW_t$. To obtain the equilibrium (steady-state) probability density $\rho(X) = (1/Z) \exp\left[-\frac{E[X]}{k_B T}\right]$ we must have that

$$QQ^T = -LC - C^T L^T.$$

This follows since $C_t = \langle X_t X_t^T \rangle := \mathbb{E}[X_t X_t^T]$ satisfies by Ito's Lemma

$$\begin{aligned} dC_t &= \langle dX_t X_t^T \rangle + \langle X_t dX_t^T \rangle + \langle dX_t dX_t^T \rangle = \left(L \langle X_t X_t^T \rangle + \langle X_t X_t^T \rangle L^T + QQ^T \right) dt \\ &= \left(LC_t + C_t^T L^T + QQ^T \right) dt. \end{aligned}$$

At steady-state we have $dC_t \rightarrow 0$ and $C_t \rightarrow C_*$ which gives

$$0 = LC_* + C_*^T L^T + QQ^T.$$

Consequence for modeling: If we know the equilibrium fluctuations have covariance structure C then the fluctuation-dissipation principle can be used to determine Q for how to thermally force the system.

Stochastic Eulerian Lagrangian Methods (SELMs) for Fluid-Structure Interactions

Fluid Equations

$$\rho \frac{\partial \mathbf{u}}{\partial t} = \mathcal{L} \mathbf{u} + \Lambda [\Upsilon (\mathbf{v} - \Gamma \mathbf{u})] + \lambda + \mathbf{f}_{\text{thm}}$$

$$\nabla \cdot \mathbf{u} = 0$$

Microstructure Equations

$$\frac{d\mathbf{X}}{dt} = \mathbf{v}$$

$$m \frac{d\mathbf{v}}{dt} = -\Upsilon (\mathbf{v} - \Gamma \mathbf{u}) - \nabla_{\mathbf{X}} \Phi[\mathbf{X}] + \zeta + \mathbf{F}_{\text{thm}}$$

Energy and Dissipation

$$E[u, v, \mathbf{X}] = \frac{1}{2} \rho \int_{\Omega} \|\mathbf{u}(x)\|^2 dx + \frac{1}{2} m \|\mathbf{v}\|^2 + \Phi(\mathbf{X})$$

$$L = \begin{bmatrix} \rho^{-1} (\mathcal{L} - \Lambda \Upsilon \Gamma) & \rho^{-1} \Lambda \Upsilon \\ m^{-1} \Upsilon \Gamma & -m^{-1} \Upsilon \end{bmatrix}$$

$$QQ^T = -LC - C^T L^T$$

$$\rho(\cdot) = (1/Z) \exp \left[-\frac{E[\cdot]}{k_B T} \right]$$

$$C = \begin{bmatrix} \rho^{-1} k_B T \delta(x-y) & 0 \\ 0 & m^{-1} k_B T \delta_{ij} \end{bmatrix}$$

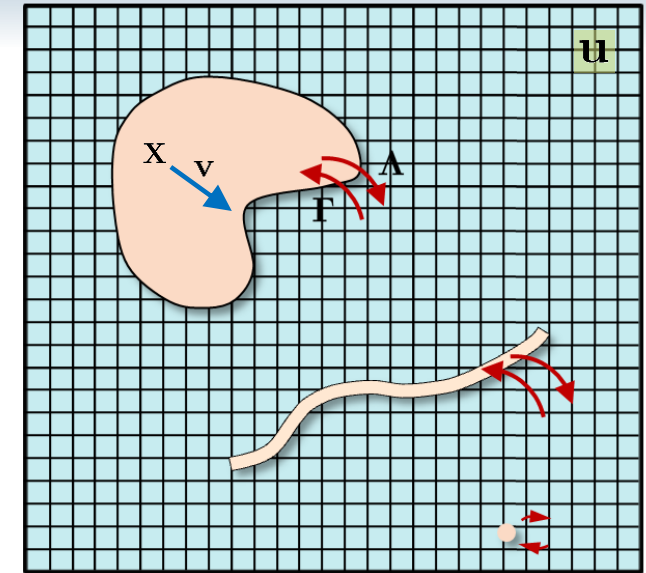
Thermal Fluctuations

$$\langle \mathbf{f}_{\text{thm}}(s) \mathbf{f}_{\text{thm}}^T(t) \rangle = -(2k_B T) (\mathcal{L} - \Lambda \Upsilon \Gamma) \delta(t-s)$$

$$\langle \mathbf{F}_{\text{thm}}(s) \mathbf{F}_{\text{thm}}^T(t) \rangle = (2k_B T) \Upsilon \delta(t-s)$$

$$\langle \mathbf{f}_{\text{thm}}(s) \mathbf{F}_{\text{thm}}^T(t) \rangle = -(2k_B T) \Lambda \Upsilon \delta(t-s)$$

Eulerian-Lagrangian Approach



Operators:

- \mathcal{L} \longrightarrow Fluid dissipation (viscosity).
- Υ \longrightarrow Structure "slip" relative to local flow field.
- Γ \longrightarrow Kinematic particle velocity for given flow.
- Λ \longrightarrow Induced fluid force density from particle.

Notation:

- $\mathbf{u} = \mathbf{u}(\mathbf{x}, t)$ \longrightarrow Fluid velocity.
- $\mathbf{X} = \mathbf{X}(\mathbf{q}, t)$ \longrightarrow Structure configuration
- $\mathbf{v} = \mathbf{v}(\mathbf{q}, t)$ \longrightarrow Structure velocity.

Coupling Operators

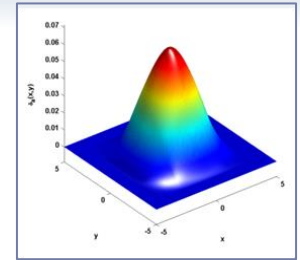
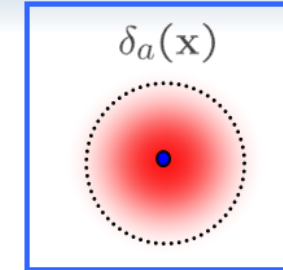
Fluid-Structure Interaction Models

Coupling Operators: Immersed Boundary Approach

Conservation of total momentum

$$\int_{\Omega} (\Lambda \mathbf{F})(\mathbf{x}) d\mathbf{x} = \int_{\mathcal{S}} \mathbf{F}(\mathbf{q}) d\mathbf{q}$$

└──────────┬──────────> “integrates to one.”



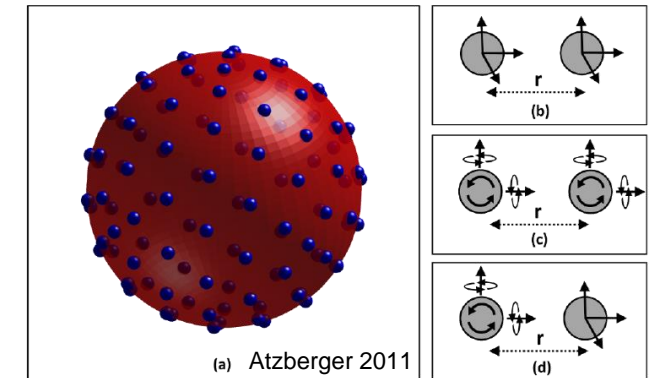
Peskin 2002

Peskin delta-function

Conservation of energy

(overdamped limit)

$$E[\mathbf{u}, \mathbf{X}] = \frac{1}{2} \int \rho |\mathbf{u}(\mathbf{y})|^2 d\mathbf{y} + \Phi(\mathbf{X})$$



Operators from Faxen Relations

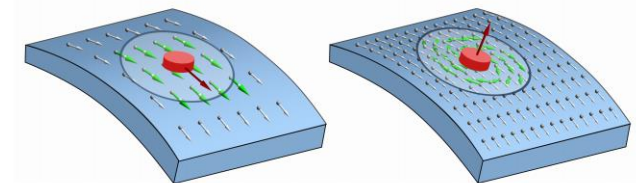
Adjoint condition

$$\int_{\mathcal{S}} (\Gamma \mathbf{u})(\mathbf{q}) \cdot \mathbf{F}(\mathbf{q}) d\mathbf{q} = \int_{\Omega} \mathbf{u}(\mathbf{x}) \cdot (\Lambda \mathbf{F})(\mathbf{x}) d\mathbf{x}$$

└──────────┬──────────> $\langle \Gamma \mathbf{u}, \mathbf{F} \rangle = \langle \mathbf{u}, \Lambda \mathbf{F} \rangle \longrightarrow \Gamma = \Lambda^T$

Non-dissipative coupling \rightarrow requires operators be **adjoints!**

Useful for **deriving operators** modeling fluid-structure interactions.



2016 Atzberger & Sigurdsson

Surface operators from reference fields

Immersed Boundary Method Coupling and Rotne-Prager-Yamakawa Couplings

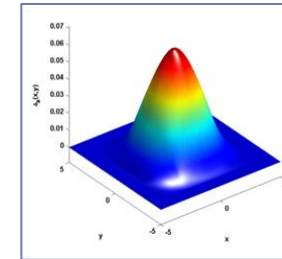
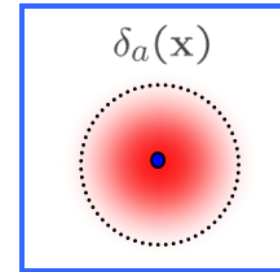
Coupling operators: Immersed Boundary Method

$$\Gamma[u] = \int \delta_a(\mathbf{x} - \mathbf{X}^{[j]}(t)) \mathbf{u}(\mathbf{x}, t) d\mathbf{x}$$

$$\Lambda[F] = \delta_a(\mathbf{x} - \mathbf{X}^{[j]}(t)) \mathbf{F}$$

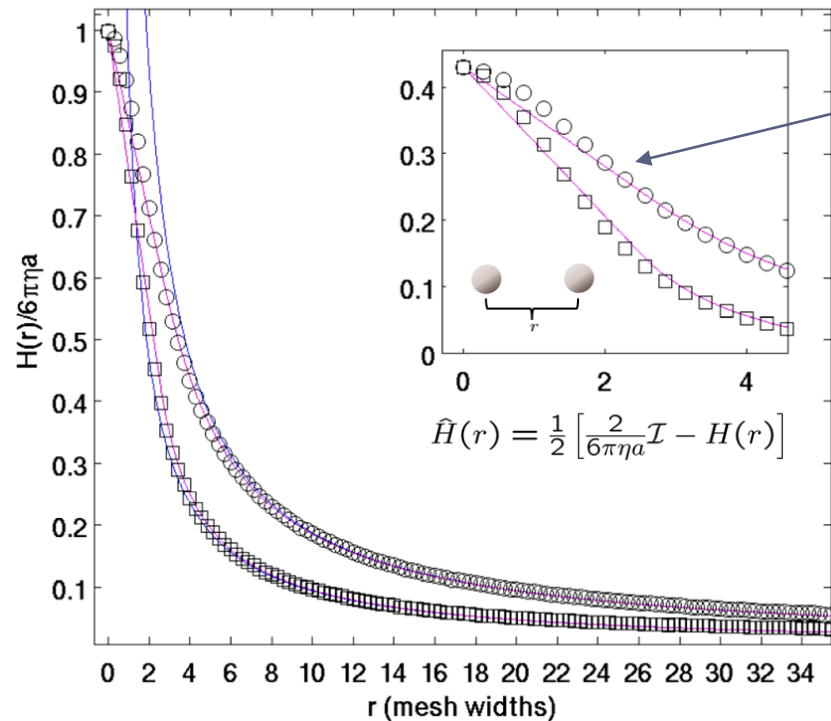
$$“\Gamma = \Lambda^T”$$

Peskin Delta-Function

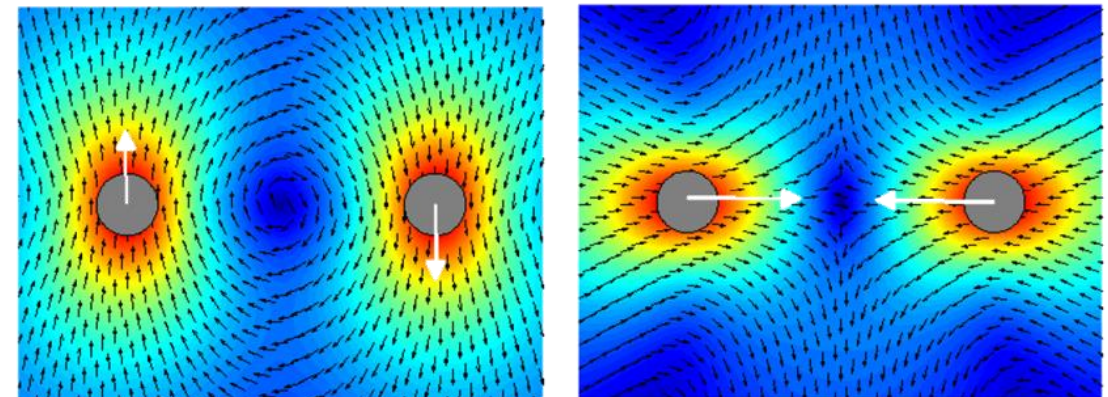


Peskin 2002

Effective IB Hydrodynamic Coupling Tensor

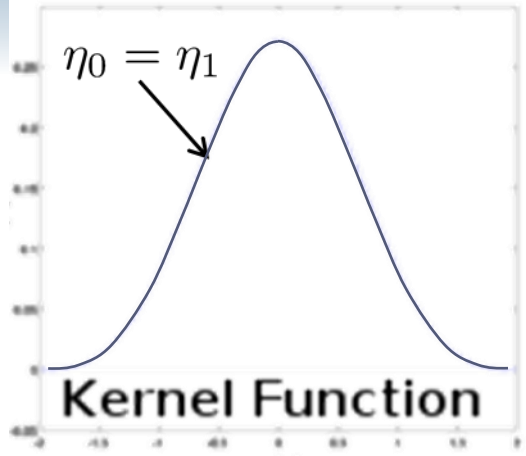
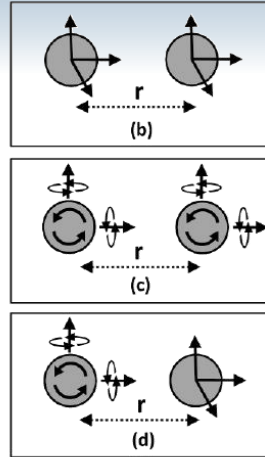
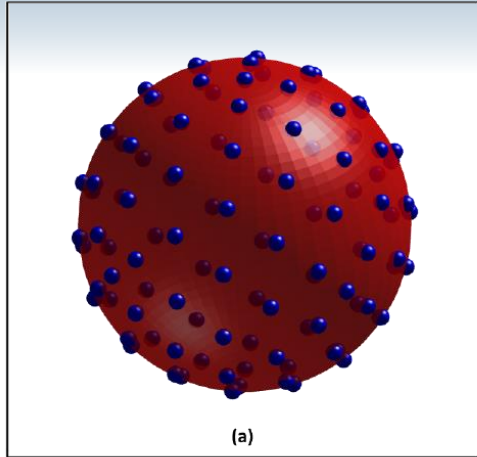


Hydrodynamic Coupling



Atzberger 2011

Coupling Operators based on Faxen Relations



Adjoint condition

$$\int_{\mathcal{S}} (\Gamma \mathbf{u})(\mathbf{q}) \cdot \mathbf{F}(\mathbf{q}) d\mathbf{q} = \int_{\Omega} \mathbf{u}(\mathbf{x}) \cdot (\Lambda \mathbf{F})(\mathbf{x}) d\mathbf{x}$$

$$\langle \Gamma \mathbf{u}, \mathbf{F} \rangle = \langle \mathbf{u}, \Lambda \mathbf{F} \rangle$$

$$“\Gamma = \Lambda^T”$$

Faxen Kinematic Relations $\rightarrow \Gamma$:

$$\Gamma_0 \mathbf{u} = \sum_{\mathbf{m}} \langle \eta_0(\mathbf{y}_{\mathbf{m}} - (\mathbf{X}_{\text{cm}} + \mathbf{z})) \mathbf{u}_{\mathbf{m}} \rangle_{\tilde{\mathcal{S}}, |\mathbf{z}|=R} \Delta x_{\mathbf{m}}^3$$

$$\Gamma_1 \mathbf{u} = \frac{3}{2R^2} \sum_{\mathbf{m}} \langle \eta_1(\mathbf{y}_{\mathbf{m}} - (\mathbf{X}_{\text{cm}} + \mathbf{z})) (\mathbf{z} \times \mathbf{u}_{\mathbf{m}}) \rangle_{\tilde{\mathcal{S}}, |\mathbf{z}|=R} \Delta x_{\mathbf{m}}^3.$$

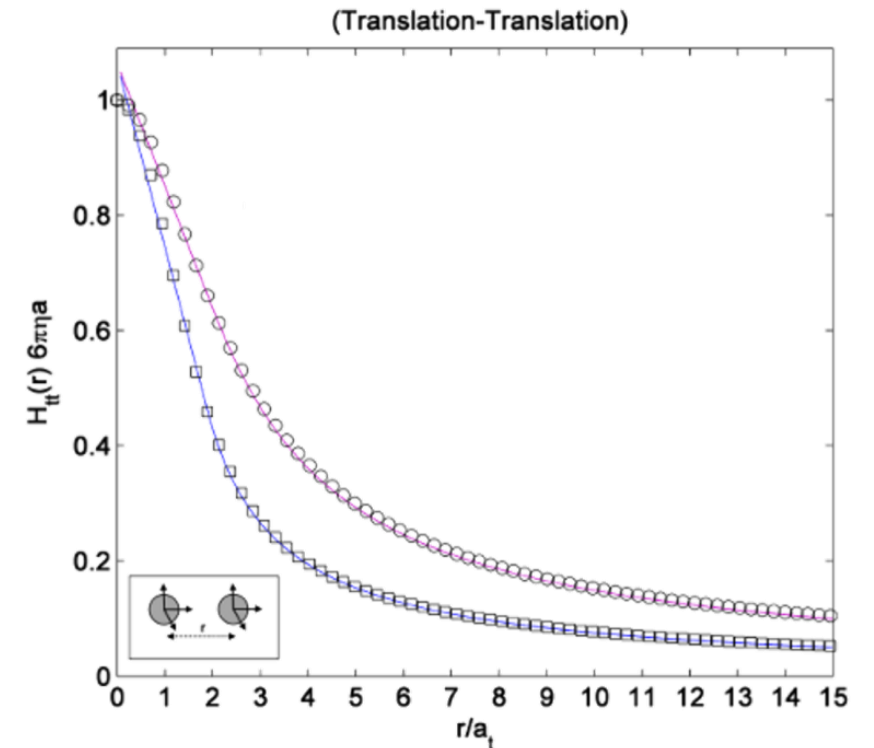
Adjoint Condition $\rightarrow \Lambda$:

$$\Lambda_0(\mathbf{x}_{\mathbf{m}}) = \left(\langle \eta_0(\mathbf{x}_{\mathbf{m}} - (\mathbf{X}_{\text{cm}} + \mathbf{z})) \rangle_{\tilde{\mathcal{S}}, |\mathbf{z}|=R} \right) \mathbf{F}$$

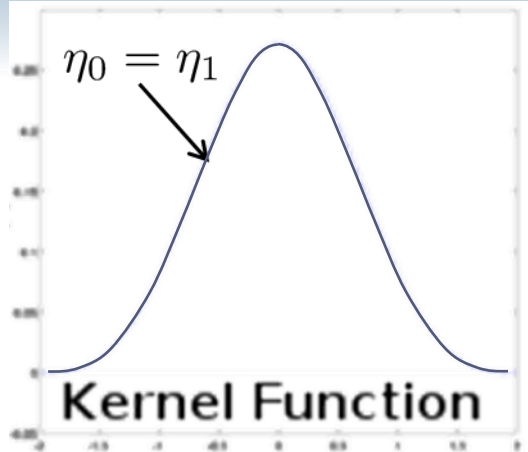
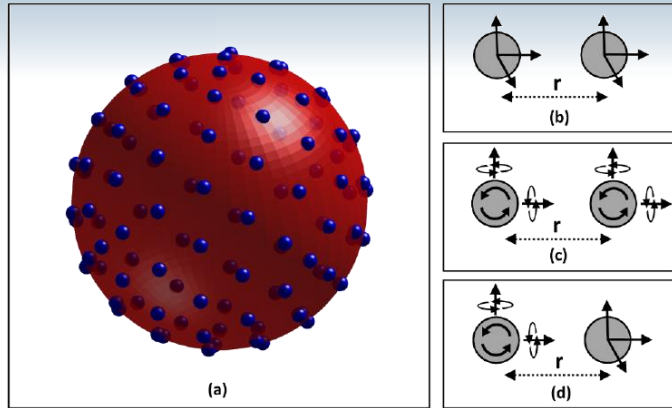
$$\Lambda_1(\mathbf{x}_{\mathbf{m}}) = -\frac{3}{2R^2} \left(\langle \mathbf{z} \eta_1(\mathbf{x}_{\mathbf{m}} - (\mathbf{X}_{\text{cm}} + \mathbf{z})) \rangle_{\tilde{\mathcal{S}}, |\mathbf{z}|=R} \right) \times \mathbf{T}.$$

Atzberger 2011

<http://atzberger.org/>



Coupling Operators based on Faxen Relations



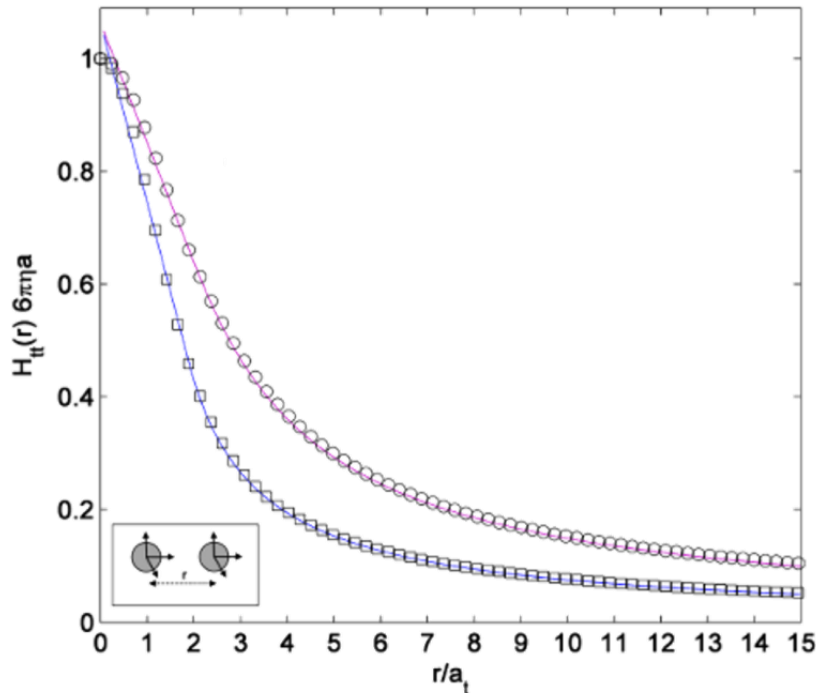
Adjoint condition

$$\int_{\mathcal{S}} (\Gamma \mathbf{u})(\mathbf{q}) \cdot \mathbf{F}(\mathbf{q}) d\mathbf{q} = \int_{\Omega} \mathbf{u}(\mathbf{x}) \cdot (\Lambda \mathbf{F})(\mathbf{x}) d\mathbf{x}$$

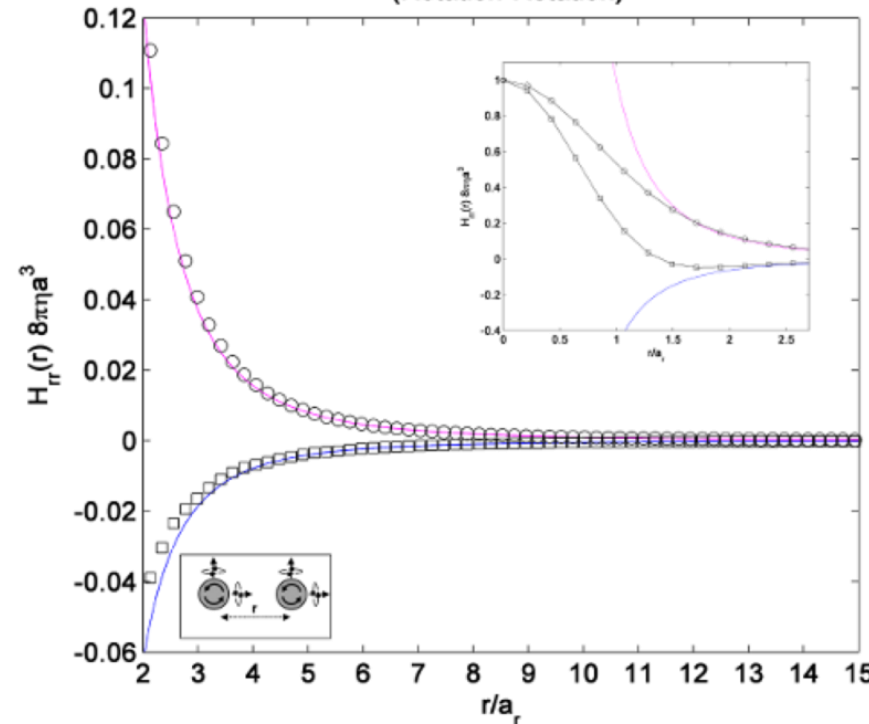
$$\langle \Gamma \mathbf{u}, \mathbf{F} \rangle = \langle \mathbf{u}, \Lambda \mathbf{F} \rangle$$

$$“\Gamma = \Lambda^T”$$

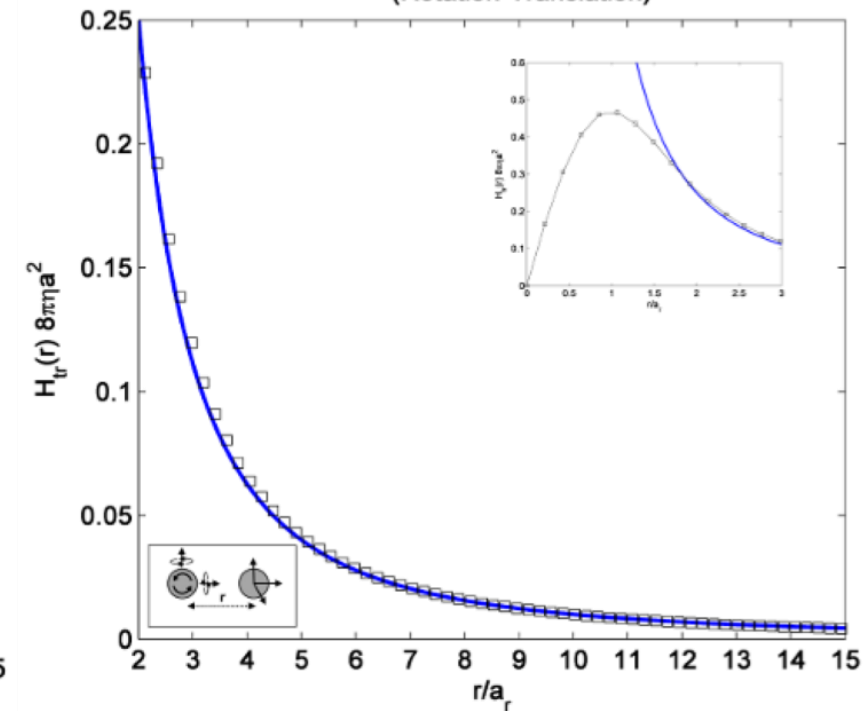
(Translation-Translation)



(Rotation-Rotation)



(Rotation-Translation)

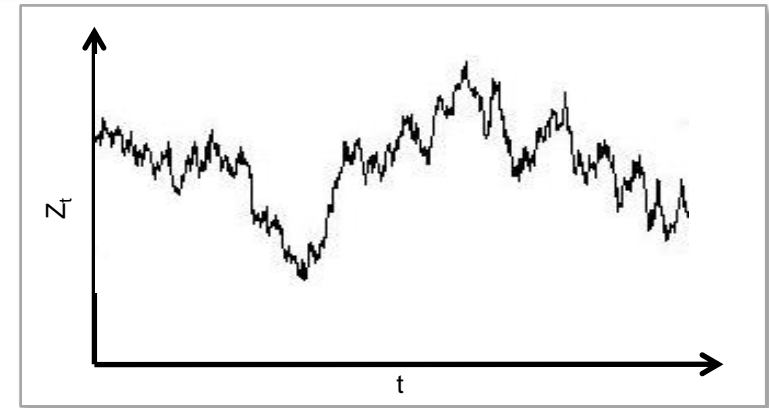


Excellent agreement for $r > 2a$! Atzberger 2011

Fluid-Structure Interactions Subject to Thermal Fluctuations A Few Physical Regimes

Time-Scales of Dynamics and Numerical Stiffness

Time-scales	
Fluid Modes	Particle Diffusion
$\tau_\lambda = \frac{\rho}{4\pi^2\mu} \lambda^2$	$\tau_{\text{diff}}(a) \approx \frac{a^2}{D_a}$
$\lambda = 10\text{nm} : \tau = 10^{-3}\text{ns}$	$\tau_{\text{diff}}(1\text{nm}) \approx 10^0\text{ns}$
$\lambda = 1000\text{nm} : \tau = 10\text{ns}$	$\tau_{\text{diff}}(10\text{nm}) \approx 10^3\text{ns}$



Stiffness

Thermal fluctuations excite all fluid modes.

For regime I formulation (additional sources):

- microstructure inertia
- fluid-structure slip $-\Upsilon(\mathbf{v} - \Gamma\mathbf{u})$

Elasticity of microstructures.

Equilibration time-scales of system vary over wide range.

Approaches

- Perturbation analysis of SPDEs : reduced descriptions.
- Develop stiff stochastic time-step integrators.

Model Reduction for Stochastic Systems

Stochastic differential equation:

$$d\mathbf{Z}(t) = \mathbf{a}(\mathbf{Z}(t))dt + \mathbf{b}(\mathbf{Z}(t))d\mathbf{W}_t \longrightarrow \mathcal{A}_\epsilon = \mathbf{a} \cdot \frac{\partial}{\partial \mathbf{z}} + \frac{1}{2} \mathbf{b} \mathbf{b}^T : \frac{\partial^2}{\partial \mathbf{z}^2}$$

Backward-Kolomogorov PDE:

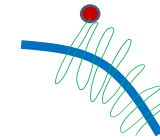
$$\begin{aligned} \frac{\partial u}{\partial t} &= \mathcal{A}_\epsilon u \\ u(x, 0) &= f(x) \end{aligned} \longrightarrow u(x, t) = E^{x,0} [f(X_t)]$$

Perturbation Analysis:

$$u(\mathbf{z}, t) = u_0(\mathbf{z}, t) + u_1(\mathbf{z}, t)\epsilon + u_2(\mathbf{z}, t)\epsilon^2 \cdots + u_n(\mathbf{z}, t)\epsilon^n + \cdots$$

Split operator into “slow” and “fast” parts: $\mathbf{z} = (\mathbf{z}_s, \mathbf{z}_f)$ **invariant distribution**

$$\mathcal{A}_\epsilon = L_{slow} + L_{fast} \longrightarrow L_{fast} = \frac{1}{\epsilon} (L_2 + \epsilon \tilde{L}_2), \quad L_2^* \Psi = 0, \int \Psi d\mathbf{z}_f = 1$$



average drift part

remainder

$$\longrightarrow L_{slow} = \bar{L}_1 + L_1 \longrightarrow \bar{L}_1 = \int \Psi(\mathbf{z}_f | \mathbf{z}_s) L_{slow} d\mathbf{z}_f, \quad L_1 = L_{slow} - \bar{L}_1$$

$$\mathcal{A}_\epsilon = \bar{L}_1 + \epsilon L_\epsilon, \quad L_\epsilon = \frac{1}{\epsilon} (L_1 + \tilde{L}_2) + \frac{1}{\epsilon^2} L_2$$

$\epsilon \rightarrow 0$: compare orders

$$\mathcal{A} = \bar{L}_1 + \epsilon \bar{L}_0 \quad \text{leading order dynamics.} \quad \bar{L}_0 = - \int \Psi (L_1 + \tilde{L}_2) L_2^{-1} L_1 d\mathbf{z}_f$$

Reduced dynamics:

$$\mathcal{A} = \tilde{\mathbf{a}} \cdot \frac{\partial}{\partial \mathbf{z}} + \frac{1}{2} \tilde{\mathbf{b}} \tilde{\mathbf{b}}^T : \frac{\partial^2}{\partial \mathbf{z}^2} \longrightarrow d\tilde{\mathbf{Z}}_t = \tilde{\mathbf{a}}(\tilde{\mathbf{Z}}_t)dt + \tilde{\mathbf{b}}(\tilde{\mathbf{Z}}_t)d\tilde{\mathbf{W}}_t$$

Summary of Regimes for SELMs

Stochastic Eulerian Lagrangian Methods (SELMs)

Fluid dynamics:

$$\rho \frac{\partial \mathbf{u}}{\partial t} = \mu \Delta \mathbf{u} - \nabla p + \Lambda [\Upsilon(\mathbf{v} - \Gamma \mathbf{u})] + \mathbf{f}_{\text{thm}}$$

$$\nabla \cdot \mathbf{u} = 0$$

Structure dynamics:

$$\frac{d\mathbf{X}}{dt} = \mathbf{v}$$

$$m \frac{d\mathbf{v}}{dt} = -\Upsilon(\mathbf{v} - \Gamma \mathbf{u}) - \nabla_{\mathbf{X}} \Phi[\mathbf{X}] + \zeta + \mathbf{F}_{\text{thm}}$$

Thermal Fluctuations

$$\langle \mathbf{f}_{\text{thm}}(s) \mathbf{f}_{\text{thm}}^T(t) \rangle = -(2k_B T) (\mu \Delta - \Lambda \Upsilon \Gamma) \delta(t - s)$$

$$\langle \mathbf{F}_{\text{thm}}(s) \mathbf{F}_{\text{thm}}^T(t) \rangle = (2k_B T) \Upsilon \delta(t - s)$$

$$\langle \mathbf{f}_{\text{thm}}(s) \mathbf{F}_{\text{thm}}^T(t) \rangle = -(2k_B T) \Lambda \Upsilon \delta(t - s).$$

Microstructure density matched with fluid

Fluid-structure dynamics:

$$m \ll \rho \ell^3$$

$$\frac{d\mathbf{p}}{dt} = \rho^{-1} \mathcal{L} \mathbf{p} + \Lambda [-\nabla_{\mathbf{X}} \Phi(\mathbf{X})] - (\nabla_{\mathbf{X}} \cdot \Lambda) k_B T + \lambda + \mathbf{g}_{\text{thm}}$$

$$\frac{d\mathbf{X}}{dt} = \rho^{-1} \Gamma \mathbf{p} + \Upsilon^{-1} [-\nabla_{\mathbf{X}} \Phi(\mathbf{X})] + \zeta + \mathbf{G}_{\text{thm}}$$

$$\nabla_{\mathbf{X}} \cdot \Lambda = \text{Tr}[\nabla_{\mathbf{X}} \Lambda]$$

Phase space compressibility (p, X).

Thermal Fluctuations:

$$\langle \mathbf{g}_{\text{thm}}(s) \mathbf{g}_{\text{thm}}^T(t) \rangle = -(2k_B T) \mathcal{L} \delta(t - s)$$

$$\langle \mathbf{G}_{\text{thm}}(s) \mathbf{G}_{\text{thm}}^T(t) \rangle = (2k_B T) \Upsilon^{-1} \delta(t - s)$$

$$\langle \mathbf{g}_{\text{thm}}(s) \mathbf{G}_{\text{thm}}^T(t) \rangle = 0.$$

- Structure momentum no longer tracked.
- Removes a source of stiffness.
- Non-conjugate Hamiltonian formulation yields metric-factor in phase-space.

Microstructure-fluid no-slip coupling (S-Immersed-Boundary)

Fluid-Structure Equations:

$$\Upsilon \rightarrow \infty$$

$$\frac{d\mathbf{p}}{dt} = \rho^{-1} \mathcal{L} \mathbf{p} + \Lambda [-\nabla_{\mathbf{X}} \Phi(\mathbf{X})] + (\nabla_{\mathbf{X}} \cdot \Lambda) k_B T + \lambda + \mathbf{g}_{\text{thm}}$$

$$\frac{d\mathbf{X}}{dt} = \rho^{-1} \Gamma \mathbf{p}$$

Thermal Fluctuations:

$$\langle \mathbf{g}_{\text{thm}}(s) \mathbf{g}_{\text{thm}}^T(t) \rangle = -(2k_B T) \mathcal{L} \delta(t - s).$$

- Structure dynamics no-longer inertial.
- Removes additional sources of stiffness.
- Regime of the Stochastic Immersed Boundary Method.
- Phase-space metric reflected in the drift term.

Microstructure-fluid stress balance

Fluid-Structure Equations:

$$\mu \rightarrow \infty$$

$$\frac{d\mathbf{X}}{dt} = H_{\text{SELM}} [-\nabla_{\mathbf{X}} \Phi(\mathbf{X})] + (\nabla_{\mathbf{X}} \cdot H_{\text{SELM}}) k_B T + \mathbf{h}_{\text{thm}}$$

$$H_{\text{SELM}} = \Gamma (-\varphi \mathcal{L})^{-1} \Lambda$$

Thermal Fluctuations:

$$\langle \mathbf{h}_{\text{thm}}(s) \mathbf{h}_{\text{thm}}^T(t) \rangle = (2k_B T) H_{\text{SELM}} \delta(t - s).$$

- Fluid momentum no longer tracked.
- Balance of hydrodynamic stresses with elastic stresses.
- Removes additional sources of stiffness.
- Regime of the Stokesian-Brownian Dynamics (Brady 1980, McCammond 1980's).
- Phase-space metric reflected in the drift term.

Spatial and Temporal Discretizations

Fluctuation-Dissipation Balance

Stochastic Immersed Boundary Method

Fluid-structure equations

Fluid:

$$\rho \frac{D\mathbf{u}(\mathbf{x}, t)}{Dt} = \mu \Delta \mathbf{u}(\mathbf{x}, t) - \nabla p(\mathbf{x}, t) + \mathbf{F}_{\text{prt}}(\mathbf{x}, t)$$

$$\nabla \cdot \mathbf{u}(\mathbf{x}, t) = 0.$$

Microstructure:

$$\frac{d\mathbf{X}^{[j]}(t)}{dt} = \int \delta_a(\mathbf{x} - \mathbf{X}^{[j]}(t)) \mathbf{u}(\mathbf{x}, t) d\mathbf{x}$$

$$\mathbf{F}_{\text{ptr}}(\mathbf{x}, t) = \sum_{j=1}^M \mathbf{F}^{[j]} \delta_a(\mathbf{x} - \mathbf{X}^{[j]}(t))$$

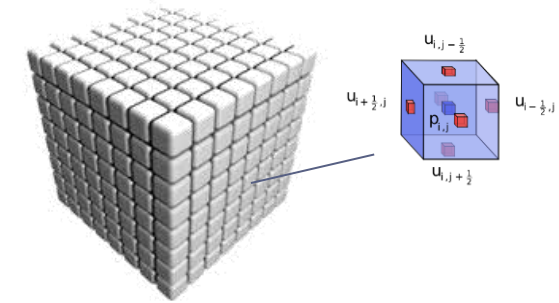
Thermal fluctuations

$$\mathbf{F}_{\text{thm}}(\mathbf{x}, t) = \mathbf{F}_{\text{drift}}(\mathbf{x}, t) + \mathbf{F}_{\text{stoch}}(\mathbf{x}, t) \sim \text{Gaussian}$$

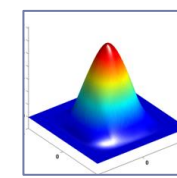
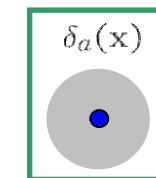
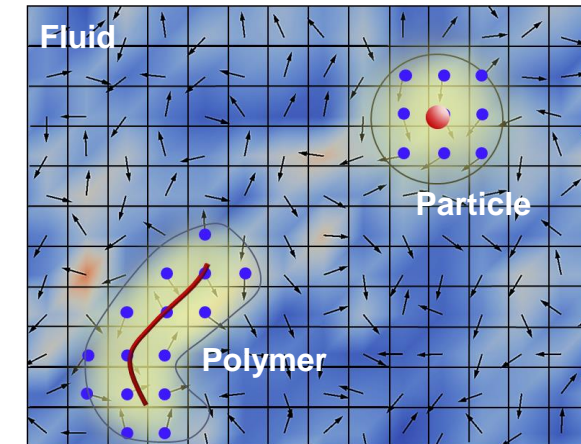
$$\langle \mathbf{F}_{\text{stoch}}(\mathbf{x}, t) \mathbf{F}_{\text{stoch}}^T(\mathbf{y}, s) \rangle = -2k_B T \mu \Delta \delta(\mathbf{x} - \mathbf{y}) \delta(t - s)$$

$$\mathbf{F}_{\text{drift}} = -k_B T \sum_{j=1}^M \nabla_{\mathbf{X}^{[j]}} \delta_a(\mathbf{x} - \mathbf{X}^{[j]}(t))$$

Numerical Discretization

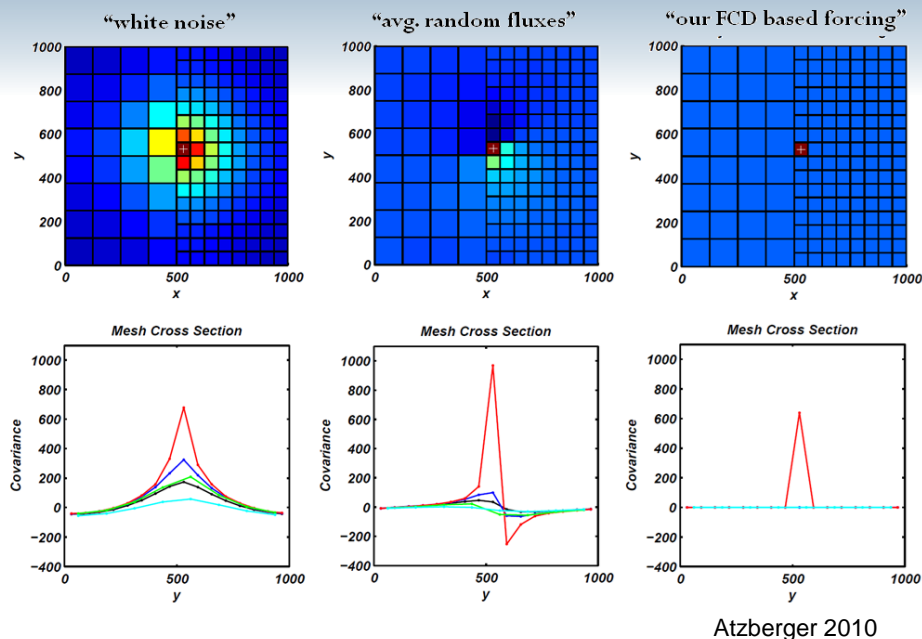
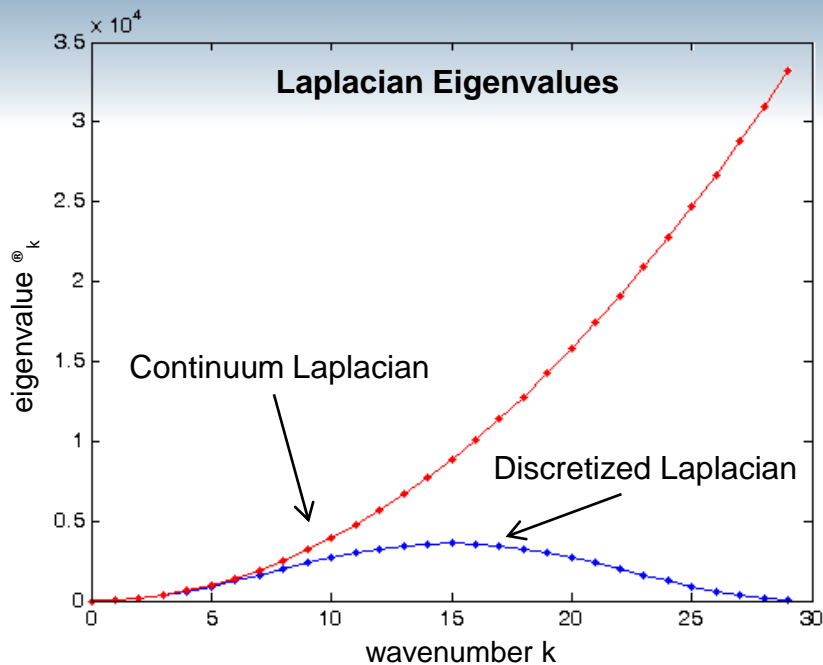


Fluid-Structure Coupling

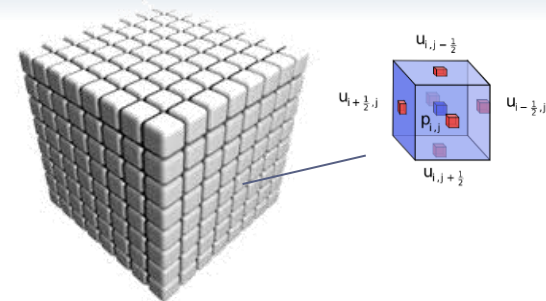


Peskin 1972, Atzberger, Peskin, Kramer 2007, Atzberger, Tabak 2015

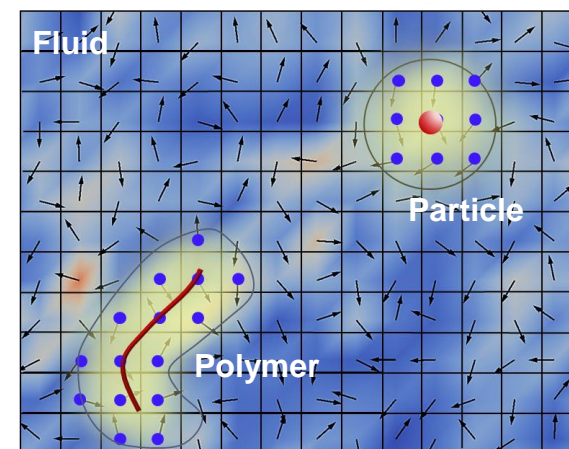
Numerical Methods and Spatial Discretization



Numerical Discretization



Fluid-Structure Coupling



Dissipation rates **not the same** for continuum and discrete system.

Thermal forcing should be based on the spatial discretization method.

Fluctuation-dissipation-based discretizations

$$Lu \leftarrow \Delta u \quad [Lu]_i^{(\ell)} = \sum_k \frac{u_{i+e_k}^{(\ell)} - 2u_i^{(\ell)} + u_{i-e_k}^{(\ell)}}{\Delta x^2}$$

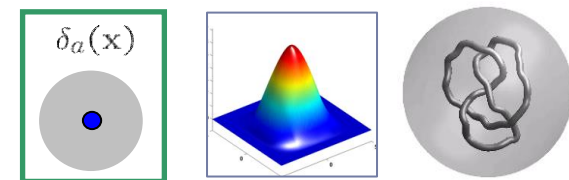
$$E[u] = \frac{1}{2} \rho \sum_i u_i^2 \Delta x^3 \quad \rho(u) = (1/Z) \exp \left[\frac{E[u]}{k_B T} \right]$$

$$C_{ij} \leftarrow \frac{k_B T}{\rho \Delta x^3} \delta_{ij}$$

$$\langle \mathbf{f}_{\text{thm}}(s) \mathbf{f}_{\text{thm}}^T(t) \rangle = - (LC + CL^T) \delta(t - s)$$

Papers on methods for:

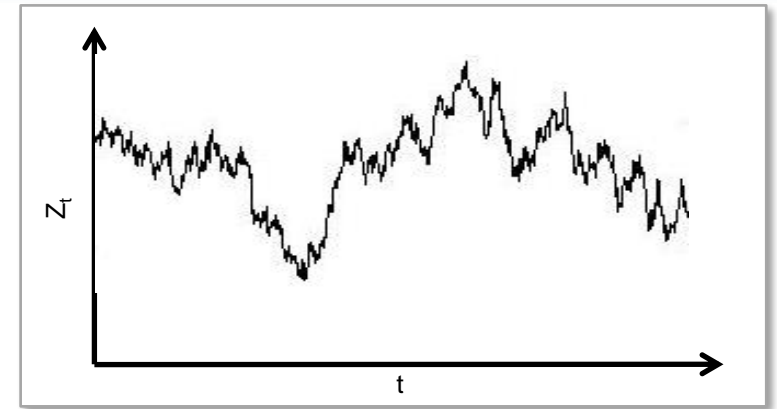
- **Finite Difference Methods** (Peskin, Kramer, Atzberger 2007).
- **Adaptive Meshes** (Atzberger 2010).
- **Finite Element Methods** (Plunkett, Pazner, Atzberger 2014, 2019).
- **Meshless Methods** (Gross, Atzberger 2020).



Peskin 1972, Atzberger, Peskin, Kramer 2007, Atzberger, Tabak 2015

Time-Scales of Dynamics and Numerical Stiffness

Time-scales	
Fluid Modes	Particle Diffusion
$\tau_\lambda = \frac{\rho}{4\pi^2\mu} \lambda^2$	$\tau_{\text{diff}}(a) \approx \frac{a^2}{D_a}$
$\lambda = 10\text{nm} : \tau = 10^{-3}\text{ns}$	$\tau_{\text{diff}}(1\text{nm}) \approx 10^0\text{ns}$
$\lambda = 1000\text{nm} : \tau = 10\text{ns}$	$\tau_{\text{diff}}(10\text{nm}) \approx 10^3\text{ns}$



Stiffness

Thermal fluctuations excite all fluid modes.

For regime I formulation (additional sources):

- microstructure inertia
- fluid-structure slip $-\Upsilon(\mathbf{v} - \Gamma\mathbf{u})$

Elasticity of microstructures.

Equilibration time-scales of system vary over wide range.

Approaches

- Perturbation analysis of SPDEs : reduced descriptions.
- Develop stiff stochastic time-step integrators.

Stiff Time-step Integrator

Fluid equations

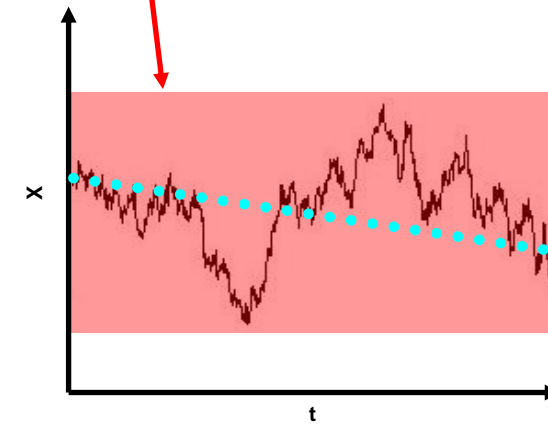
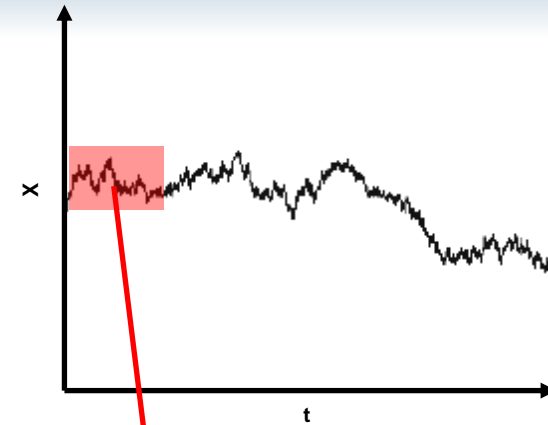
$$\begin{aligned} du &= \mathcal{L}u dt && \text{(dissipation in fluid)} \\ &+ \rho^{-1} \mathbf{F}_{\text{prt}} dt && \text{(microstructure forces)} \\ &+ Q dB_t && \text{(thermal force)} \\ \nabla \cdot \mathbf{u} &= 0 && \text{(incompressibility)} \end{aligned}$$

Structure equations

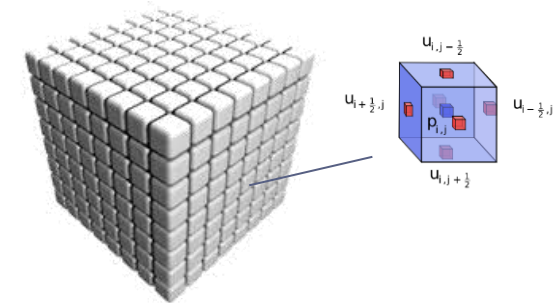
$$\begin{aligned} \frac{d\mathbf{X}^{[j]}(t)}{dt} &= \int \delta_a(\mathbf{x} - \mathbf{X}^{[j]}(t)) \mathbf{u}(\mathbf{x}, t) d\mathbf{x} \\ \mathbf{F}_{\text{prt}}(\mathbf{x}, t) &= \sum_{j=1}^M -\nabla_{\mathbf{X}^{[j]}} V(\{\mathbf{X}(t)\}) \delta_a(\mathbf{x} - \mathbf{X}^{[j]}(t)) \end{aligned}$$

Integration by exponential factor (ito calculus)

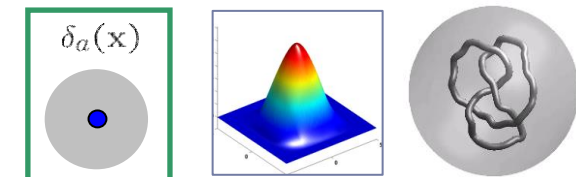
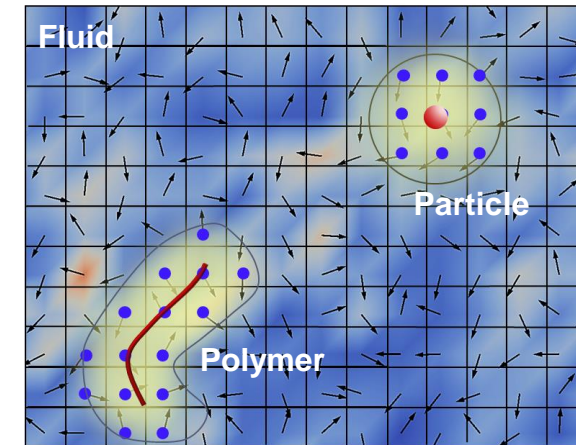
$$\mathbf{u}(t) = e^{t\mathcal{L}} \mathbf{u}(0) + \int_0^t e^{(t-s)\mathcal{L}} \rho^{-1} \mathbf{F}_{\text{prt}}(s) ds + \int_0^t e^{(t-s)\mathcal{L}} Q dB_s = e^{t\mathcal{L}} \mathbf{u}(0) + \bar{\mathbf{I}}_{\text{prt}} + \bar{\mathbf{I}}_{\text{thm}}$$



Numerical Discretization



Fluid-Structure Coupling



Stiff Time-step Integrator

Integration by exponential factor (ito calculus)

$$\mathbf{u}(t) = e^{t\mathcal{L}}\mathbf{u}(0) + \int_0^t e^{(t-s)\mathcal{L}}\rho^{-1}\mathbf{F}_{\text{prt}}(s)ds + \int_0^t e^{(t-s)\mathcal{L}}Qd\mathbf{B}_s = e^{t\mathcal{L}}\mathbf{u}(0) + \bar{\mathbf{I}}_{\text{prt}} + \bar{\mathbf{I}}_{\text{thm}}$$

Particle force

$$\mathbf{I}_{\text{prt}}(t) := \int_0^t e^{(t-s)\mathcal{L}}\rho^{-1}\mathbf{F}_{\text{prt}}(s)ds$$

Approximate by constant force

$$\hookrightarrow \mathbf{I}_{\text{prt}}(t) \approx -\rho^{-1}\mathcal{L}^{-1} [\mathcal{I} - e^{t\mathcal{L}}] \mathbf{F}_{\text{prt}}(0)$$

Thermal fluctuations

$$\mathbf{I}_{\text{thm}}(t) := \int_0^t e^{(t-s)\mathcal{L}}Qd\mathbf{B}_s$$

Ito calculus yields Gaussian with

$$\begin{aligned} \hookrightarrow \langle \mathbf{I}_{\text{thm}}(t) \rangle &= 0 \\ \langle \mathbf{I}_{\text{thm}}(t)\mathbf{I}_{\text{thm}}(t)^T \rangle &= \int_0^t e^{(t-s)\mathcal{L}}QQ^T e^{(t-s)\mathcal{L}^T} ds := \Lambda(t) \\ \Lambda_{\mathbf{k},\mathbf{k}}(t) &= -\frac{1}{2\alpha_{\mathbf{k}}} [1 - e^{-2\alpha_{\mathbf{k}}\Delta t}] Q_{\mathbf{k},\mathbf{k}}^2 \end{aligned}$$

Stiff Time-step Integrator

Integration by exponential factor (ito calculus)

$$\mathbf{u}(t) = e^{t\mathcal{L}}\mathbf{u}(0) + \int_0^t e^{(t-s)\mathcal{L}}\rho^{-1}\mathbf{F}_{\text{prt}}(s)ds + \int_0^t e^{(t-s)\mathcal{L}}Qd\mathbf{B}_s = e^{t\mathcal{L}}\mathbf{u}(0) + \bar{\mathbf{I}}_{\text{prt}} + \bar{\mathbf{I}}_{\text{thm}}$$

$$\mathbf{I}_{\text{prt}}(t) \approx -\rho^{-1}\mathcal{L}^{-1}[\mathcal{I} - e^{t\mathcal{L}}]\mathbf{F}_{\text{prt}}(0)$$

$$\Lambda_{\mathbf{k},\mathbf{k}}(t) = -\frac{1}{2\alpha_{\mathbf{k}}}[1 - e^{-2\alpha_{\mathbf{k}}\Delta t}]Q_{\mathbf{k},\mathbf{k}}^2$$

Fluid Integrator

$$\mathbf{u}^{n+1} = e^{\Delta t\mathcal{L}}\mathbf{u}^n + \mathcal{L}^{-1}[\mathcal{I} - e^{\Delta t\mathcal{L}}]\rho^{-1}\mathbf{F}_{\text{prt}}^n + \Gamma\xi^n$$

ξ is Gaussian with

$$\langle \xi \rangle = 0, \quad \langle \xi\xi^T \rangle = \mathcal{I}$$

$$\Lambda = \Gamma\Gamma^T$$

Unconditionally stable for the fluid

Accuracy depends only on structure force approximation (otherwise exact).

Requires prior knowledge of Γ .

Method **viable only if** efficient to compute $e^{\Delta t\mathcal{L}}$.

Efficient for uniform meshes (FFTs).

Stiff Time-step Integrator

Fluid equations

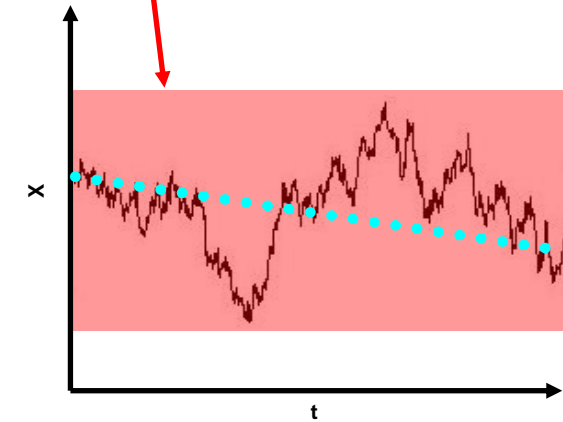
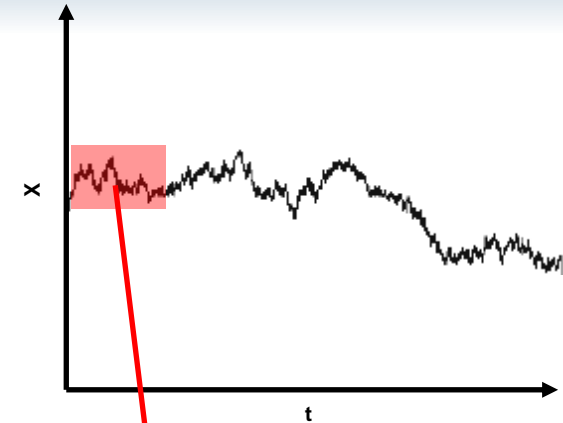
$$\begin{aligned}
 d\mathbf{u} &= \mathcal{L}\mathbf{u}dt && \text{(dissipation in fluid)} \\
 &+ \rho^{-1}\mathbf{F}_{\text{prt}}dt && \text{(microstructure forces)} \\
 &+ Qd\mathbf{B}_t && \text{(thermal force)} \\
 \nabla \cdot \mathbf{u} &= 0 && \text{(incompressibility)}
 \end{aligned}$$

Structure equations

$$\begin{aligned}
 \frac{d\mathbf{X}^{[j]}(t)}{dt} &= \int \delta_a(\mathbf{x} - \mathbf{X}^{[j]}(t))\mathbf{u}(\mathbf{x}, t)d\mathbf{x} \\
 \mathbf{F}_{\text{prt}}(\mathbf{x}, t) &= \sum_{j=1}^M -\nabla_{\mathbf{X}^{[j]}}V(\{\mathbf{X}(t)\})\delta_a(\mathbf{x} - \mathbf{X}^{[j]}(t))
 \end{aligned}$$

Integrate microstructure dynamics (ito calculus)

$$\mathbf{X}^{[j]}(t) = \mathbf{X}^{[j]}(0) + \int_0^t \int \delta_a(\mathbf{x} - \mathbf{X}^{[j]}(s))\mathbf{u}(\mathbf{x}, s)d\mathbf{x}ds \approx \mathbf{X}^{[j]}(0) + \int \delta_a(\mathbf{x} - \mathbf{X}^{[j]}(0)) \int_0^t \mathbf{u}(\mathbf{x}, s)dsd\mathbf{x}$$



Stiff Time-step Integrator

Integrate structure dynamics (ito calculus)

$$\mathbf{X}^{[j]}(t) \approx \mathbf{X}^{[j]}(0) + \int_0^t \delta_a(\mathbf{x} - \mathbf{X}^{[j]}(0)) \int_0^t \mathbf{u}(\mathbf{x}, s) ds dx$$

$$\hookrightarrow \mathbf{X}^{[j],n+1} = \mathbf{X}^{[j],n} + \int \delta_a(\mathbf{x} - \mathbf{X}^{[j],n}) \mathbf{I}_{\text{vel}}(\mathbf{x}, \Delta t) dx$$

$$\mathbf{I}_{\text{vel}}(t) := \int_0^t \mathbf{u}(s) ds$$

Integrated fluctuating fluid velocity

$\mathbf{I}_{\text{vel}}(t)$ is a Gaussian with

$$\bar{\mathbf{I}}_{\text{vel}} := \langle \mathbf{I}_{\text{vel}}(t) \rangle = \int_0^t \langle \mathbf{u}(s) \rangle ds = -\mathcal{L}^{-1} [\mathcal{I} - e^{t\mathcal{L}}] \mathbf{u}(0) + -\mathcal{L}^{-1} [t + \mathcal{L}^{-1} [\mathcal{I} - e^{t\mathcal{L}}]] \mathbf{F}_{\text{prt}}(0)$$

$$\Phi := \langle (\mathbf{I}_{\text{vel}}(t) - \bar{\mathbf{I}}_{\text{vel}}(t)) (\mathbf{I}_{\text{vel}}^T(t) - \bar{\mathbf{I}}_{\text{vel}}^T(t)) \rangle = \int_0^t \int_0^t e^{r\mathcal{L}} C e^{s\mathcal{L}^T} dr ds + \int_0^t \int_0^t \int_0^{s \wedge r} e^{(r-w)\mathcal{L}} Q Q^T e^{(s-w)\mathcal{L}^T} dw dr ds$$

$\mathbf{I}_{\text{vel}}(t)$ is correlated with $\mathbf{I}_{\text{thm}}(t)$

$$W := \langle (\mathbf{I}_{\text{vel}}(t) - \bar{\mathbf{I}}_{\text{vel}}(t)) \mathbf{I}_{\text{thm}}^T(t) \rangle = \mathcal{L}^{-1} \int_0^t e^{(t-w)\mathcal{L}} Q Q^T e^{(t-w)\mathcal{L}^T} dw + \mathcal{L}^{-1} Q Q^T \mathcal{L}^{-T} [\mathcal{I} - e^{t\mathcal{L}^T}]$$

Microstructure Integrator

$$\mathbf{X}^{[j],n+1} = \mathbf{X}^{[j],n} + \int \delta_a(\mathbf{x} - \mathbf{X}^{[j],n}) \mathbf{I}_{\text{vel}}(\mathbf{x}, \Delta t) dx$$

Stability depends now on structure forces.

Accuracy depends on

- fluid sampling approximation $\mathbf{X}(t) \sim \mathbf{X}(0)$ and structure force approximation.

Method **viable only if** efficient to compute exponentials.

Efficient for uniform meshes (FFTs).

Summary : Stiff Integrator for SIBM

Fluid Integrator

$$\mathbf{u}^{n+1} = e^{\Delta t \mathcal{L}} \mathbf{u}^n + \mathcal{L}^{-1} [\mathcal{I} - e^{\Delta t \mathcal{L}}] \rho^{-1} \mathbf{F}_{\text{prt}}^n + \Gamma \xi^n$$

ξ is Gaussian with

$$\langle \xi \rangle = 0, \quad \langle \xi \xi^T \rangle = \mathcal{I}$$

$$\Lambda = \Gamma \Gamma^T$$

Microstructure Integrator

$$\mathbf{X}^{[j],n+1} = \mathbf{X}^{[j],n} + \int \delta_a(\mathbf{x} - \mathbf{X}^{[j],n}) \mathbf{I}_{\text{vel}}(\mathbf{x}, \Delta t) d\mathbf{x}$$

$\mathbf{I}_{\text{vel}}(t)$ is a Gaussian with

$$\bar{\mathbf{I}}_{\text{vel}} := \langle \mathbf{I}_{\text{vel}}(t) \rangle = \int_0^t \langle \mathbf{u}(s) \rangle ds = -\mathcal{L}^{-1} [\mathcal{I} - e^{t\mathcal{L}}] \mathbf{u}(0) + -\mathcal{L}^{-1} [t + \mathcal{L}^{-1} [\mathcal{I} - e^{t\mathcal{L}}]] \mathbf{F}_{\text{prt}}(0)$$

$$\Phi := \langle (\mathbf{I}_{\text{vel}}(t) - \bar{\mathbf{I}}_{\text{vel}}(t)) (\mathbf{I}_{\text{vel}}^T(t) - \bar{\mathbf{I}}_{\text{vel}}^T(t)) \rangle = \int_0^t \int_0^t e^{r\mathcal{L}} C e^{s\mathcal{L}^T} dr ds + \int_0^t \int_0^t \int_0^{s \wedge r} e^{(r-w)\mathcal{L}} Q Q^T e^{(s-w)\mathcal{L}^T} dw dr ds$$

$\mathbf{I}_{\text{vel}}(t)$ is correlated with $\mathbf{I}_{\text{thm}}(t)$

$$W := \langle (\mathbf{I}_{\text{vel}}(t) - \bar{\mathbf{I}}_{\text{vel}}(t)) \mathbf{I}_{\text{thm}}^T(t) \rangle = \mathcal{L}^{-1} \int_0^t e^{(t-w)\mathcal{L}} Q Q^T e^{(t-w)\mathcal{L}^T} dw + \mathcal{L}^{-1} Q Q^T \mathcal{L}^{-T} [\mathcal{I} - e^{t\mathcal{L}^T}]$$

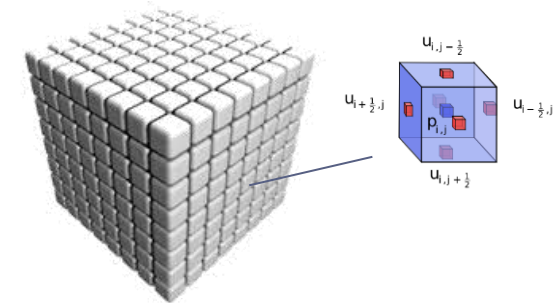
Method **viable only if** efficient to compute exponentials.

Viable for uniform meshes (FFTs).

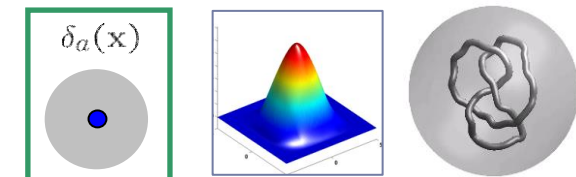
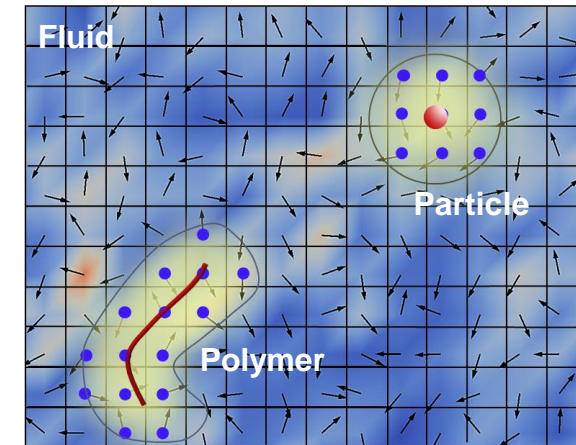
Under-resolves fluid mode dynamics and fluctuations.

Time-step limited by structure's motions.

Numerical Discretization

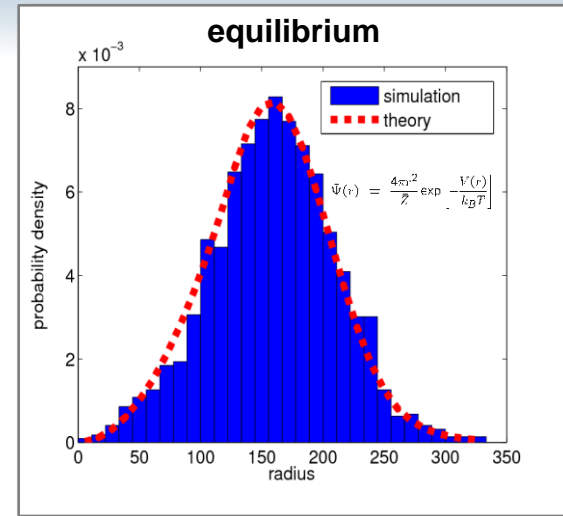
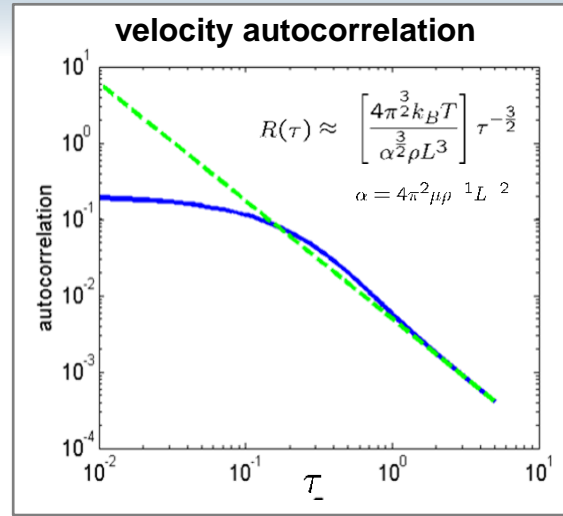
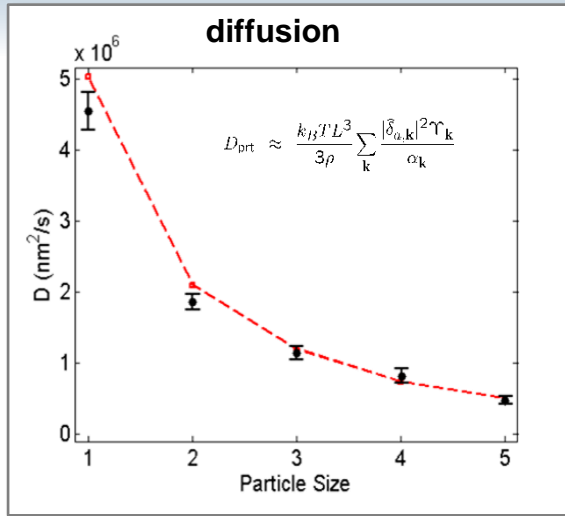


Fluid-Structure Coupling

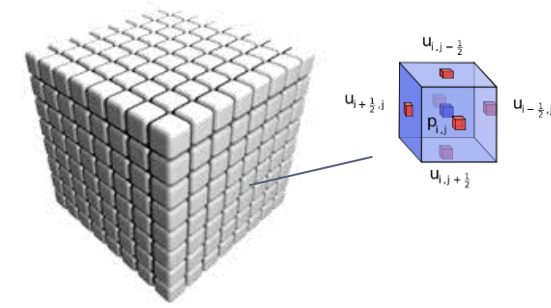


Atzberger, Peskin, Kramer 2007

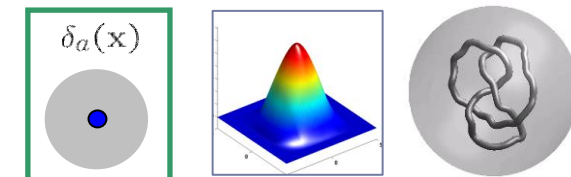
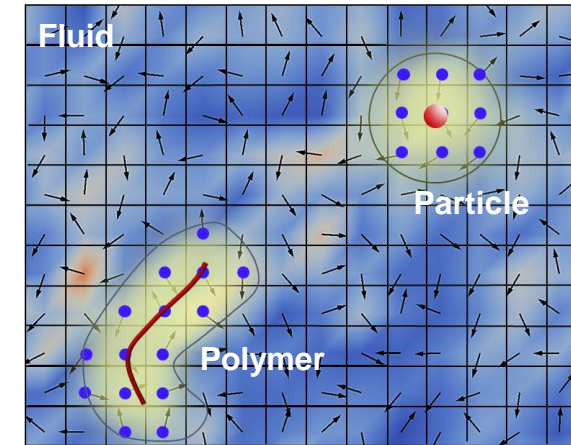
Validation of Numerical Methods for SIBM



Numerical Discretization



Fluid-Structure Coupling



Validation

Diffusivity of under-resolved particles correct.

Velocity auto-correlation has $t^{3/2}$ tail (Adler & Wainright 1950),

Auto-correlation persists from hydrodynamic “memory.”

Equilibrium configurations have Gibbs-Boltzmann statistics.

Approach can be extended to other coupling types, regimes, and numerical discretizations.

Stochastic Immersed Boundary Methods Simulations

Topology and Immersed Boundary Simulations

Topological Features

Structure motions reference a common continuum velocity field.

Solution map is homeomorphism.

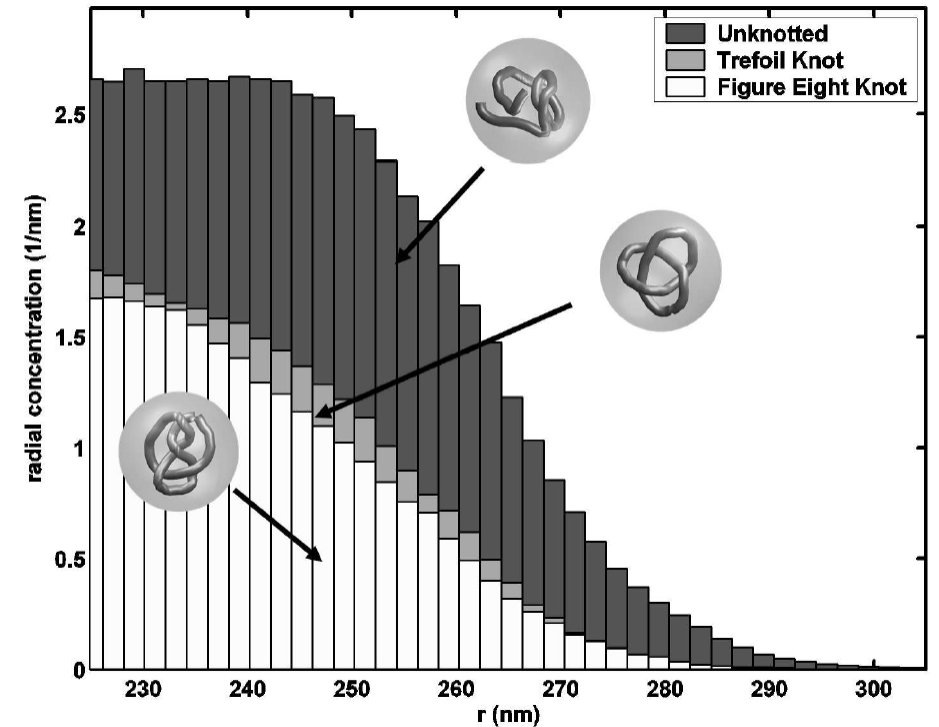
Preserves topological invariants (up to numerical error)

Knotted structures remain knotted.

Simulation: Osmotic pressures of knotted polymers.



Knot Type	Osmotic Pressure ($\text{amu}/\text{nm} \cdot \text{ns}^2$)
Unknotted	0.16
Trefoil Knot	0.0439
Figure Eight Knot	0.0392

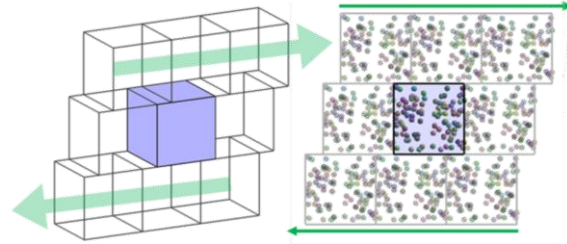


Rheological Properties and Microstructure Dynamics

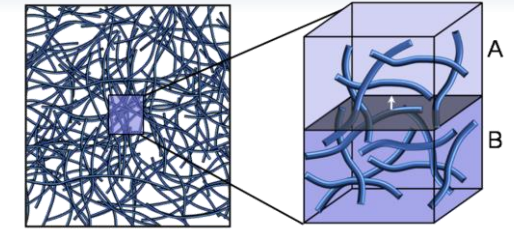
Rheometry:



Lees-Edwards Conditions:



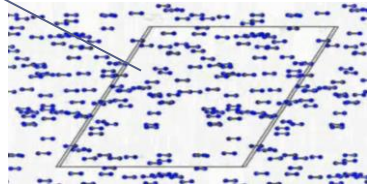
Material Stress ← Forces



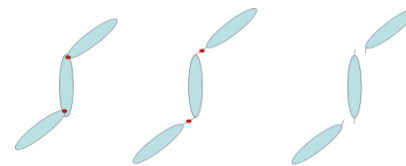
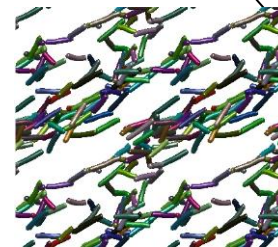
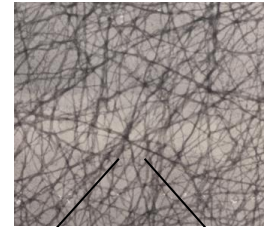
$$\sigma_{\ell,z}^{(n)} = \frac{1}{AL} \sum_{\mathbf{q} \in \mathcal{Q}_n} \sum_{j=1}^{n-1} \langle \mathbf{f}_{\mathbf{q},j}^{(\ell)} \cdot (\mathbf{x}_{q_n}^{*,(z)} - \mathbf{x}_{q_j}^{*,(z)}) \rangle$$

Polymeric Fluid (FENE)

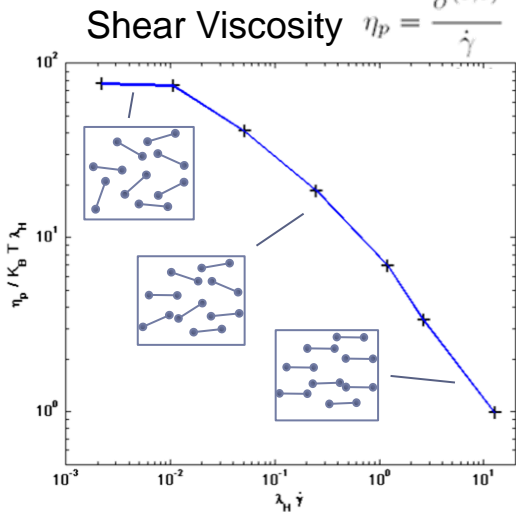
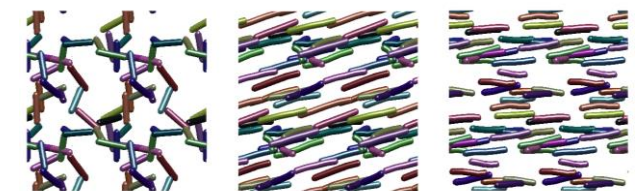
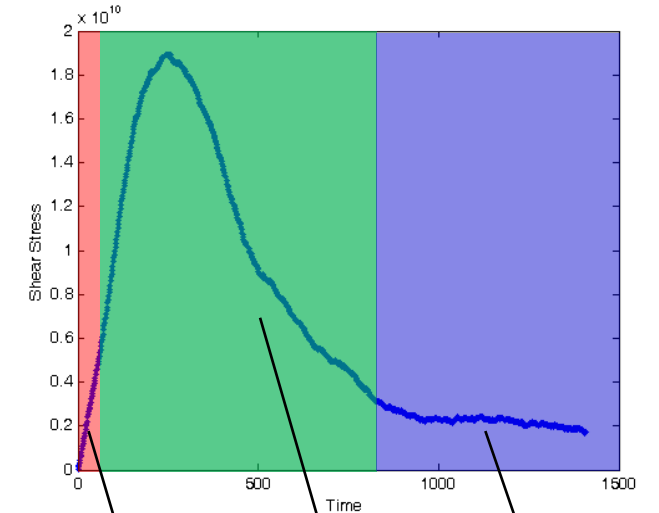
$$U(r) = \frac{K}{2} Q_0^2 \log(1 - (r/Q_0)^2)$$



Polymeric Material



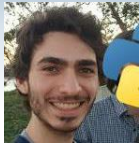
Atzberger 2013



Conclusions



B. Gross



D. Rower

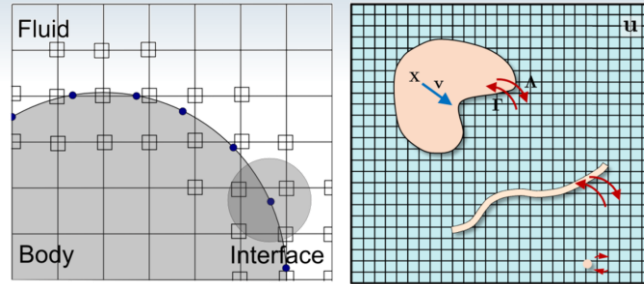


M. Padidar

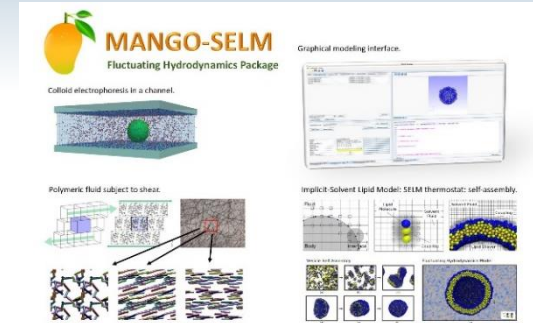


J. Sigurdsson

UCSB Recent Student
Collaborators



IB Eulerian-Lagrangian Methods



SELM Software



2016 Atzberger & Sigurdsson

Summary

Stochastic Immersed Boundary Methods with numerical solvers preserving statistical mechanics properties.

Applications in soft materials, complex fluids, rheology, microfluidics, biophysics, lipid bilayer membranes.

Surface Fluctuating Hydrodynamics for drift-diffusion dynamics of microstructures in membranes.

Software packages available for methods integrated with MD packages for simulating models (more on this later).



Papers

A Stochastic Immersed Boundary Method for Fluid-Structure Dynamics at Microscopic Length Scales,

P.J. Atzberger, P.R. Kramer, and C.S. Peskin, J. Comp. Phys., Vol. 224, Iss. 2, (2007).

Stochastic Eulerian Lagrangian Methods for Fluid Structure Interactions with Thermal Fluctuations,

P.J. Atzberger, J. of Comp. Phys., 230, pp. 2821--2837, (2011).

Surface Fluctuating Hydrodynamics Methods for the Drift-Diffusion Dynamics of Particles and Microstructures within Curved Fluid Interfaces,

D. Rower, M. Padidar, and P. J. Atzberger, arXiv:1906.01146, (2019).

Meshfree Methods on Manifolds for Hydrodynamic Flows on Curved Surfaces: A Generalized Moving Least-Squares (GMLS) Approach,

Gross B. J., Kuberry P. A., Trask N., Atzberger P. J., J. Comp. Phys., 409, 15 May (2020).

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J. K. Sigurdsson.

Funding



DOE ASCR CM4
DE-SC0009254



DOE ASCR PHILMS
DE-SC0019246



NSF Grant
DMS - 1616353



NSF CAREER Grant
DMS-0956210

More information: <http://atzberger.org/>

Publications

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P.J. Atzberger, P.R. Kramer, and C.S. Peskin, J. Comp. Phys., Vol. 224, Iss. 2, (2007). <http://dx.doi.org/10.1016/j.jcp.2006.11.015>

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<http://dx.doi.org/10.1016/j.jcp.2014.07.051>

Incorporating Shear into Stochastic Eulerian Lagrangian Methods for Rheological Studies of Complex Fluids and Soft Materials,

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