> The Navier-Stokes Equations

Ebrahim Ebrahim

Physical Principles

Conservation of Mass

Momentum Equation

The Navier-Stokes Equations

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Mass and Momentum

The Navier-Stokes equations describe the non-relativistic time evolution of **mass** and **momentum** in fluid substances.

• mass density field:
$$\rho = \rho(t, x, y, z)$$

• velocity field: $v^i = v^i(t, x, y, z), i = 1, 2, 3$

We will derive them by using **conservation of mass** and **force laws** on a control volume V. The control volume propagates in time, V = V(t).



(We will assume an isothermal continuum, so we don't need to consider energy conservation.)

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Conservation of Mass

Conservation of mass gives a continuity equation.

(Demand that the mass flux through any closed surface be the change in total mass, and use divergence theorem)

$$\dot{\rho} + \partial_i(\rho v^i) = 0$$

This provides us with nice simplifications if we later assume incompressibility

incompressibility
$$\implies \dot{\rho} = \mathbf{0} \implies \partial_i v^i = \mathbf{0}$$

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The Forces

We start by considering the forces on a control volume V.

- There are forces on the **body**, like gravity. Call this force field fⁱ.
- And there are forces on the surface of the control volume, pressures along normals and viscous forces tangentially. These are described by a stress tensor σ_{ij}.
 - σ_{ij} can be physically defined by the way it operates on a normal n^j to a surface element of area dA. It gives the force on that surface element: σ_{ij}n^jdA
 - σ_{ij} is the stress (the force per area) in the *j* direction acting on the cube face with normal in the *i* direction. Thus the diagonal components are pressures and the off-diagonal components are shear stresses.



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The Force Law

Now we write the force law on a control volume V:

$$\frac{d}{dt}\int_{V(t)}\left(\rho v^{i}\right)d^{3}x=\int_{V(t)}\left(f^{i}\right)d^{3}x+\int_{\partial V(t)}\left(\sigma^{ij}n_{j}\right)dA$$

$$rac{d}{dt}ec{
ho} = ec{
ho}_{
m body} + ec{
ho}_{
m surface}$$

Divergence theorem on the surface force term gives:

$$\frac{d}{dt}\int_{V(t)}\left(\rho v^{i}\right)d^{3}x = \int_{V(t)}\left(f^{i}\right)d^{3}x + \int_{V(t)}\left(\partial_{j}\sigma^{ij}\right)d^{3}x$$

It now remains to turn the first term into a volume integral. The time derivative cannot simply be pushed in because the volume of integration is time-dependent. The Navier-Stokes

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Reynold's Transport Theorem

We need to deal with the time derivative on $\frac{d}{dt}\int_{V(t)} \alpha(t) d^3x$ for a function $\alpha = \alpha(t, x, y, z)$ and a time-dependent volume of integration V(t).

$$\begin{split} \frac{d}{dt} \int_{V(t)} \alpha(t) &= \\ \lim_{\Delta t \to 0} \frac{1}{\Delta t} \left(\int_{V(t+\Delta t)} \alpha(t+\Delta t) - \int_{V(t)} \alpha(t) \right) &= \\ \lim_{\Delta t \to 0} \frac{1}{\Delta t} \left(\int_{V(t+\Delta t)} \alpha(t+\Delta t) - \int_{V(t)} \alpha(t+\Delta t) + \int_{V(t)} \alpha(t+\Delta t) - \int_{V(t)} \alpha(t) \right) &= \\ \lim_{\Delta t \to 0} \frac{1}{\Delta t} \left(\int_{V(t+\Delta t)} \alpha(t+\Delta t) - \int_{V(t)} \alpha(t+\Delta t) \right) + \int_{V(t)} \frac{\partial \alpha}{\partial t} &= \\ \lim_{\Delta t \to 0} \frac{1}{\Delta t} \left(\int_{\Delta V} \alpha(t+\Delta t) \right) + \int_{V(t)} \frac{\partial \alpha}{\partial t} \end{split}$$

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Reynold's Transport Theorem

The integral over the difference in volume, $\int_{\Delta V} \alpha(t + \Delta t)$, can be expressed in terms of an integral of the changes in volume over the surface.



The differential volume change at dA is $v^j n_j \Delta t \ dA$.

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Reynold's Transport Theorem

$$\lim_{\Delta t \to 0} \frac{1}{\Delta t} \left(\int_{\Delta V} \alpha(t) \right) =$$

$$\lim_{\Delta t \to 0} \frac{1}{\Delta t} \left(\sum_{\text{cube at each dA}} \alpha(\text{center of cube}) (\Delta V_{\text{at patch dA}}) \right) =$$

$$\lim_{\Delta t \to 0} \frac{1}{\Delta t} \left(\sum_{\text{cube at each dA}} \alpha(\text{center of cube}) v^j n_j \Delta t \ dA \right) =$$

$$\sum_{\text{cube at each dA}} \alpha(\text{center of cube}) v^j n_j \ dA =$$

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$$\int_{\partial V(t)} \alpha(t) v^j n_j \ dA$$

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And so we have Reynold's transport theorem:

$$\frac{d}{dt}\int_{V(t)}\alpha(t)=\int_{\partial V(t)}\alpha(t)v^{j}n_{j}\ dA+\int_{V(t)}\frac{\partial\alpha}{\partial t}$$

We can use it on the force equation:

$$\int_{\partial V(t)} \left(\rho v^{i} v^{j} n_{j} \right) dA + \int_{V(t)} \frac{\partial \left(\rho v^{i} \right)}{\partial t} = \int_{V(t)} f^{i} + \int_{V(t)} \partial_{j} \sigma^{ij}$$

Then use divergence theorem again, and combine the volume integrals:

$$\int_{V(t)} \left(\partial_j \left(\rho v^i v^j \right) + \frac{\partial \left(\rho v^i \right)}{\partial t} - f^i - \partial_j \sigma^{ij} \right) = 0$$

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Since this holds for any control volume, we get the differential form of the equation. We can also use mass conservation $\dot{\rho} = -\partial_j(\rho v^j) = -\partial_j\rho v^j - \rho \partial_j v^j$

$$\partial_{j} \left(\rho v^{i} v^{j} \right) + \frac{\partial \left(\rho v^{i} \right)}{\partial t} - f^{i} - \partial_{j} \sigma^{ij} = 0$$

$$\partial_{j} \rho v^{i} v^{j} + \rho \partial_{j} v^{i} v^{j} + \rho v^{i} \partial_{j} v^{j} + \dot{\rho} v^{i} + \rho \dot{v}^{i} - f^{i} - \partial_{j} \sigma^{ij} = 0$$

$$\partial_{j} \rho v^{i} v^{j} + \rho \partial_{j} v^{i} v^{j} + \rho v^{i} \partial_{j} v^{j} - \partial_{j} \rho v^{i} v^{j} - \rho v^{i} \partial_{j} v^{j} + \rho \dot{v}^{i} - f^{i} - \partial_{j} \sigma^{ij} = 0$$

And we are finally left with the **Cauchy momentum** equation:

$$\rho \partial_j \mathbf{v}^i \mathbf{v}^j + \rho \dot{\mathbf{v}}^i - f^i - \partial_j \sigma^{ij} = \mathbf{0}$$

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To get an actual equation we must choose a form for the stress tensor $\sigma^{ij}.$

$$\rho \partial_j \mathbf{v}^i \mathbf{v}^j + \rho \dot{\mathbf{v}}^i - f^i - \partial_j \sigma^{ij} = \mathbf{0}$$

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